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Hut-like pillar array Si Solar Cells

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Abstract

A good texturing pattern for solar cells needs to combine low Reflectance over a large wavelength range and low surface recombination to maximise the output. Nanowire and pyramid patterns offer low Reflectance in the longer and shorter wavelength regions respectively. This paper introduces an exciting new “hut” like texturing pattern with excellent performance, improving that of nanowires and pyramids; over the long and short wavelength ranges respectively. Furthermore, we analyse the effect of different structural parameters such as height, diameter, Surface Coverage (SC) and ϑ , on the solar cell performance.

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Keywords: Photovoltaic; Texturing; Silicon; Optical properties.

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1. Introduction

The incident light reflected at an interface between two media with different refractive indices has been studied for various applications (Flowers, 1975). Some examples of these applications are: Fabry-Perot lasers (Hodgson and Weber, 2003), Bragg gratings (Hill and Meltz, 1997), optical couplers (Biswas, 2003) and solar cells (Luque and Hegedus, 2011; Hamakawa, 2010), etc. In particular, solar cells have drawn a lot of their attention due to environmental benefits (Luque and Hegedus, 2011). Some of the techniques that scientists have developed to reduce the Reflectance from the solar cell surface are: deposition of anti-reflection coatings (Yan et al., 2013), exploiting plasmonic properties (Spinelli et al., 2012), texturing of various patterns on the solar cell surface (Baker-Finch and McIntosh, 2011; Mavrokefalos, 2012), etc.

These techniques attempt to improve the transmission at the air-silicon interface by different means. In the case of anti reflection coating technique, the transmission can improve up to 8% (Yan et al., 2013). However, it requires a very precise layer deposition. In addition, the frequency dependant nature of refractive indices makes it less attractive to developers (Yan et al., 2013). In the case of plasmonics, the transmission can increase up to 9%. The operation at the resonance frequency of the metal enables the re-emission of incident light into the substrate (Spinelli et al., 2012). However, the large solar spectrum is not efficiently utilized due to the very narrow bandwidth of the plasmonic behaviour (Spinelli et al., 2012).

The lowering of the Reflectance in texturing patterns such as pyramids (Baker-Finch and McIntosh, 2011; Mavrokefalos et al., 2012), nanowires (Garnett and Yang, 2010; Madaria et al., 2011) or micro pillars arrays (Yoon et al., 2012; Shin et al., 2012; Logeeswaran et al.,

2010; Kim et al., 2013; Sinton et al., 1996) is caused by certain factors. One factor is the refractive index averaging between the air and the cell material. A second factor is the light trapping by multiple reflections of the incoming light (Mavrokefalos et al., 2012; Garnett and Yang, 2010; Madaria et al., 2012; Shin et al., 2012; Logeeswaran et al., 2010).

A common issue between texturing patterns is the high level of surface recombination due to a high surface recombination velocity enhanced by defects. In combination with the dominance of the surface effects due to the high surface-to-volume ratio (Dan et al., 2011; Chang et al., 1993). This may worsen the electrical performance of the solar cell regardless how good the optical performance is (Dan et al., 2011; Green, 1982; Toor et al., 2011; Li et al., 2011; Shir et al., 2010). Furthermore, high levels of surface recombination can lead to a short life span for the material. A way to reduce it is called “surface passivation” (Dan et al., 2011). It consists on oxidizing the Silicon at high temperatures which reduces the carrier lifetime (Schmidt et al., 2001). Furthermore, surface passivation is challenging to achieve due to the high precision required at this small dimension (Dan et al., 2011). This shows the importance of finding ways to reduce Reflectance with low surface-to-volume ratio.

In the case of the “hut” like structure, it is possible to optimize light trapping further than other patterns. This is due to strong E field intensity near the substrate in-between pillars. In addition, the light trapped in-between the huts, by multiple reflections, is incident on the hut at angles that improve absorption. Furthermore, it shows good optical performance for small dimensions which is an advantage regarding surface recombination. In the following sections, we discuss in detail the effect of structural parameters of this “hut” like pattern. In section 2 we discuss the structure of the “hut” like pattern and the methodology, section 3 compares the performance of the hut-like and other available patterns, section 4 analyses in detail the effect on the performance of surface coverage, ϑ , overlapped pattern, height, cap and we identify an appropriate set of parameters and our conclusions are presented in section 5.

2. The hut like pattern and methodology

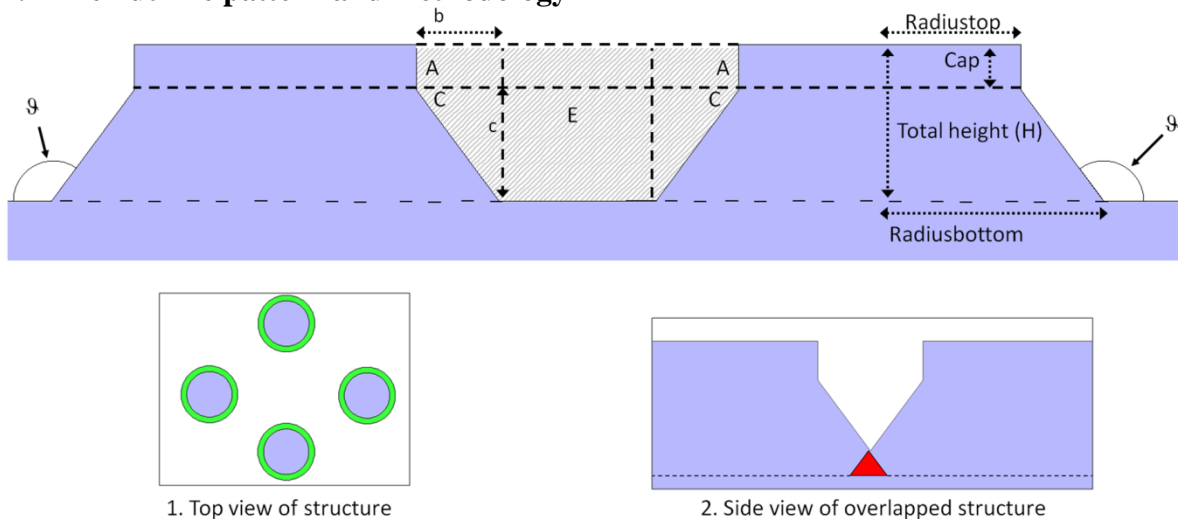


Fig. 1. Schematic of proposed hut-like micro pillar array.

A schematic diagram of the “hut” like pattern is presented in Fig.1. The purpose of this pattern is to enhance light trapping in-between huts by multiple reflections. This is achieved by an optimization of the air volume between the huts. This is a similar concept to other patterns such as nanowires or micro pillars. Further benefits of the hut like pattern are discussed in later sections.

Inset 1 in Fig. 1 has a top view of the pattern where we can see the hexagonal configuration of the pattern. The inner circle (i.e. purple) corresponds to the vertical section of the pillar and outer circle (i.e. green) corresponds to the sloped part of the huts. This sloped part is important for improved light trapping of the pattern enabling higher absorption of the incident light as well as improved trapping due to multiple reflections. We will discuss this in more detail in section 4.1.

There are some critical factors to be considered: Surface Coverage (SC), the angle ϑ , Cap and the area between the huts (see Fig. 1). The SC is defined as follows:

$$SC = \frac{2\pi \cdot \text{radius}_{\text{top}}^2 \cdot 100}{\text{simulation window}} \quad (1)$$

where $\text{radius}_{\text{top}}$ is the radius corresponding to the top of the hut. The simulation window is the finite area of solar cell being simulated (we apply Periodic Boundary Conditions (PCB) in the x and y directions). Furthermore, the angle ϑ (in degrees ($^{\circ}$)) is calculated as follows:

$$\vartheta = \frac{180 \cdot \tan^{-1}\left(\frac{H}{\text{radius}_{\text{bottom}} - \text{radius}_{\text{top}}}\right)}{\pi} \quad (2)$$

where total height is the length measured from the substrate to the top of the hut and $\text{radius}_{\text{bottom}}$ is the radius corresponding to the bottom of the hut. The area in-between huts can be easily calculated as the sum of the areas A, C and E which are shaded in Fig. 1:

$$A = \text{Cap} \cdot b \quad (3)$$

$$C = 1/2 \cdot c \cdot b \quad (4)$$

$$E = \text{distance between huts} \cdot H \quad (5)$$

$$\text{Area} = 2A + 2C + E = E + 2(A + C) \quad (6)$$

Substituting Eq. 3, 4 and 5 into Eq. 6 we obtain the following expression:

$$\text{Area} = \text{distance between huts} \cdot H + 2 \cdot b \left(\text{Cap} + \frac{1}{2} \cdot c \right) \quad (7)$$

By rearranging the equation it is also possible to express the area in-between huts in terms of H, Cap, ϑ , SC, $\text{radius}_{\text{top}}$ and $\text{radius}_{\text{bottom}}$ as follows:

$$\text{Area} = H \cdot \left(\frac{H}{\tan\left(\frac{\vartheta\pi}{180}\right)} \cdot \left(\frac{\text{Cap}}{H} + 1 \right) + \sqrt{12 \cdot \text{radius}_{\text{bottom}}^2 - \frac{\sqrt{3} \cdot 2\pi \cdot \text{radius}_{\text{top}}^2 \cdot 100}{SC}} \right) \quad (8)$$

To obtain the impact of these structural parameters on Reflectance, we run simulations using FDTD solutions (Lumerical Solutions, 2015). This package solves Maxwell’s equations by the Finite Difference Time Domain (FDTD) method (Yee, 1966). The light

source launches a plane wave with the 1.5 AM solar spectrum. Above the source we record any reflected waves from the pattern. Throughout the paper we use the Reflectance integrated over all wavelengths to compare performances for different parametric set up. Reflectance is defined as:

$$R = \frac{\int_{I_{AM1.5}} T(\lambda) \cdot I_{AM1.5}(\lambda) d\lambda}{\int_{I_{AM1.5}} I_{AM1.5}(\lambda) d\lambda} \quad (9)$$

where R , T , $I_{AM1.5}$ and λ are the Reflectance, the transmission air-silicon interface, the reference solar spectrum and the wavelength respectively. In the next section we compare the performance of the hut-like with the performance of other patterns.

3. Comparison with other patterns

The hut-like texturing pattern offers the possibility of an optical performance with a low R . This attractive benefit is complemented by dimensions offering a low surface recombination. In Fig. 2 we compare the R of the optimized hut-like pattern with that of some other available texturing patterns such as: vertical micro pillars (Cabrera-Espana et al., 2014), nanowires (Wang et al., 2011) and pyramids (Hou et al., 2012; Papet et al., 2006).

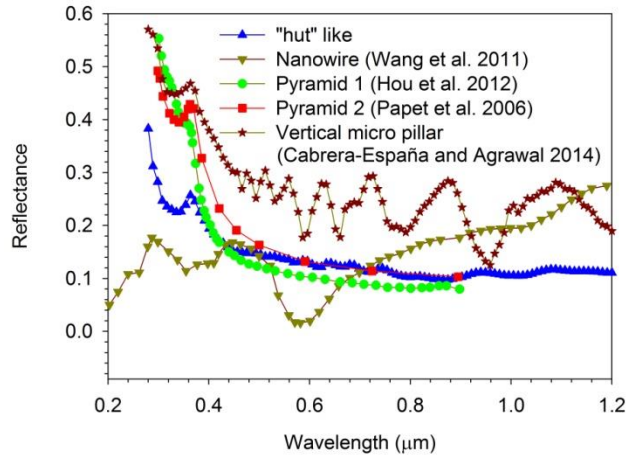


Fig. 2. Performance comparison of hut-like structure with other texturing patterns.

From this figure we can see the wavelength dependent performance of the hut-like pattern. Low R is achieved by maximizing the effect of the multiple reflections as well as increasing the first time absorption. In Sec. 4.1 we describe how this is optimized using θ and SC . Other texturing patterns have similar approach to optimizing multiple reflections but with different results. As we can see in the figure, the hut-like provides a lower R for the entire solar spectrum compared to vertical micro pillars. When we compare it with the performance of the nanowires, we see lower R for the hut-like for longer wavelength. While comparing with the pyramids, the hut-like pattern offers lower R in the shorter wavelength range. We attribute the improved performance of the hut-like pattern to more effective light trapping. This is especially significant since no back reflector has been used to increase further the light path.

The excellent performance of the pattern compared to the others proves the potential of this structure to lower R. In the next section we introduce and analyse the effect on the R of different structural parameters.

4. Results

In this section we discuss in detail the effect of different parameters on R beginning with the effect of the area in-between huts.

4.1 Effect of area in-between huts on Reflectance, SC and ϑ

Light trapping takes place in the area in-between huts hence an appropriate choice of SC and ϑ is important for the best performance. An intuitive way of varying this area is to change the distance between huts (i.e. SC). This is in line with our findings on vertical micro pillar arrays (Cabrera-Espana et al., 2014) where we have discussed in detail the impact of varying SC.

The hut-like pattern offers an alternative way to vary the area in-between huts: by changing ϑ (see Fig. 1). As we increase ϑ from vertical micro pillar (i.e. $\vartheta=90^\circ$), keeping the rest of the parameters constant, we change the area in-between huts and also the angle of incidence of light on the sloped part. As a consequence, R changes. In addition, the Fresnel reflection at low angle of incidence is high and as the angle of incidence increases, it reaches a minimum. Further increase in the angle of incidence will lead R to increase. Therefore there is a range of ϑ optimizing the absorption on the slope part of the huts.

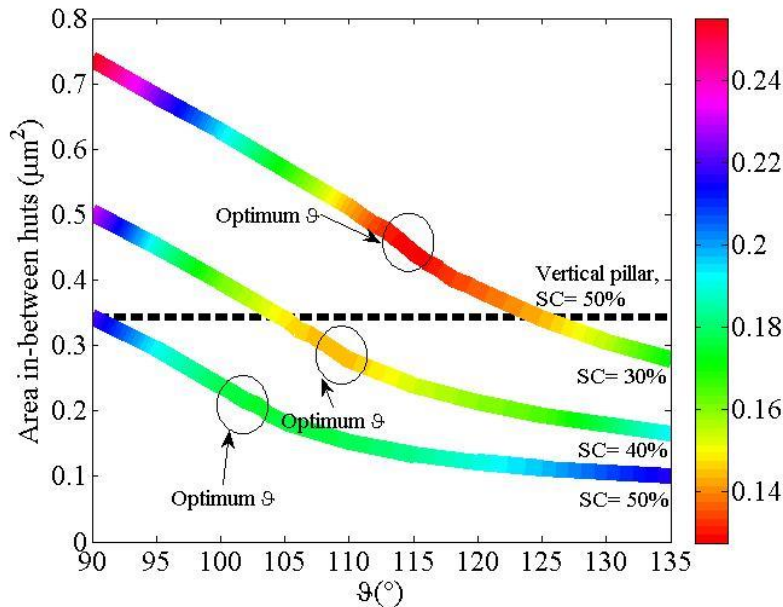


Fig. 3. Angular performance, Area in-between the huts vs ϑ for $H = 1 \mu\text{m}$, $\text{Radiustop} = 0.5 \mu\text{m}$ and $\text{Cap} = 0.2 \mu\text{m}$ where the line colour represents the R.

Consequently, we need to take into account both ways of changing the area (i.e. varying SC and ϑ). Figure 3 shows the R dependence (see colour bar) with variation of the area between huts (y axis) and ϑ (x axis). We show three lines for SC=30, 40 and 50%

respectively and have indicated the optimum ϑ for each. For reference we have included a dashed line for vertical micro pillars ($\vartheta=90^\circ$) with $H=1\mu\text{m}$ and $SC=50\%$.

There is a similar trend in all three cases: area in-between huts effectively determines the light concentration. For any given SC , when ϑ increases from 90° , first there is a decrease in R . This is identified by the colour of the lines changing towards green ($SC=50\%$), yellow ($SC=40\%$) and red ($SC=30\%$), reaching a minimum at optimum ϑ .

Further increase in ϑ , leads to an increase in R , identified by the change in colour towards blue ($SC=50\%$), green ($SC=40\%$) and yellow ($SC=30\%$) end of the spectrum. This increase is consequence of overlap in the pattern (inset 2, Fig. 1): there is an effective decrease in H . Furthermore, this decrease is dependent on ϑ . As we vary ϑ , there is a change in the area in-between huts. This change affects the amount of light penetrating in the area in-between huts as well as the multiple reflections. Therefore, we conclude that there is a range of ϑ optimizing both the absorption and multiple reflections in-between huts; enhancing absorption further.

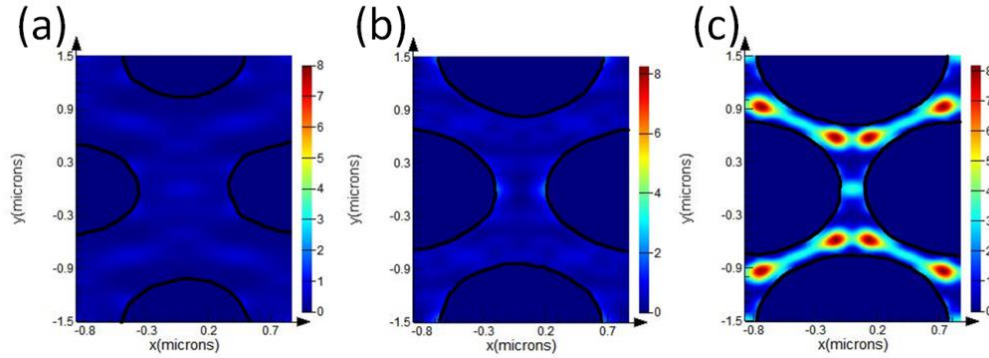


Fig. 4. Cross section showing E field intensity at $0.2\mu\text{m}$ above the substrate for structure with $H=1\mu\text{m}$, $Cap=0.2\mu\text{m}$ and $SC=30\%$ at $\lambda \approx 0.373\mu\text{m}$ for (a): $\vartheta=90^\circ$. (b): $\vartheta=105^\circ$. (c): $\vartheta=115^\circ$.

In Figs. 4 a, b and c we show the E field intensity at $0.2\mu\text{m}$ above the substrate for different values of ϑ ($\vartheta=90^\circ$, $\vartheta=115^\circ$ and $\vartheta=105^\circ$) for constant $SC=30\%$. The black lines indicate the edge of the hut circumference. There is a clear increase in the E field intensity when ϑ increases from 90° to optimum ($\vartheta=115^\circ$) due to the optimization of absorption at the slope and the multiple reflections simultaneously. As a consequence, we can see a higher E field intensity near the substrate for the optimum ϑ . These results clearly indicate the value of moving from vertical pillar to the hut-like structure. However, the trend of reducing R , as we reduce H when the pattern is overlapped seems to collapse. In the following section we explain the impact of H on R in detail.

4.2 Effect of Height on Reflectance

Figure 5 shows a performance comparison for the cases of $H=1, 2$ and $3\mu\text{m}$. For reference we include results for the vertical micro pillar for $H=1\mu\text{m}$. Keeping SC constant we change area in-between huts by changing H : for fixed Cap increase in H leads to the sloped portion being larger. We see that R decreases as H increases for a given ϑ . This is inline from Sec. 4.1 where we showed that light falling on the sloped part shows lower R .

Nevertheless, increasing H to very large values would not provide a significant benefit. This is due to the impact of the height softening as H increases. For example, from Fig. 5 we can see that the difference in R between $H= 2$ and $3 \mu\text{m}$ is smaller than the difference between $H= 1$ and $2 \mu\text{m}$. Furthermore, patterns with large H may suffer high levels of surface recombination.

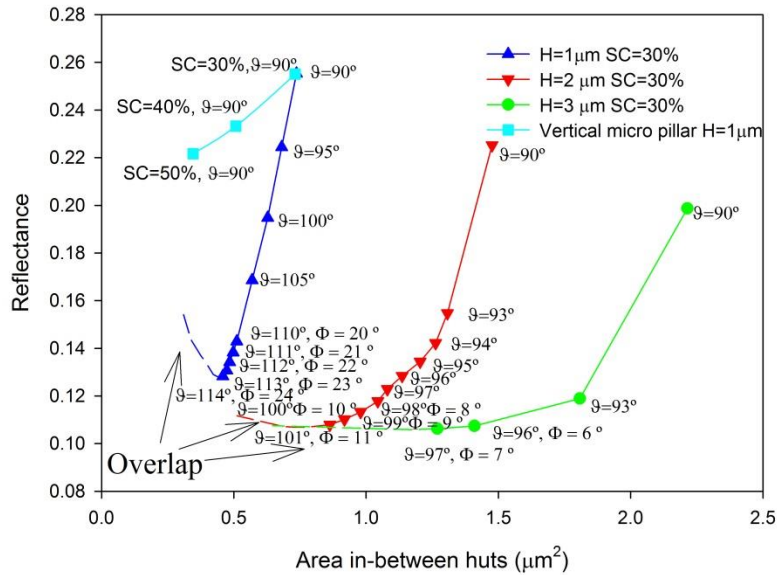


Fig. 5. Variation in R as the area in-between huts changes, for different H .

Another parameter related to H is the Cap which we discuss in the following section.

4.3 Effect of Cap on the Reflectance

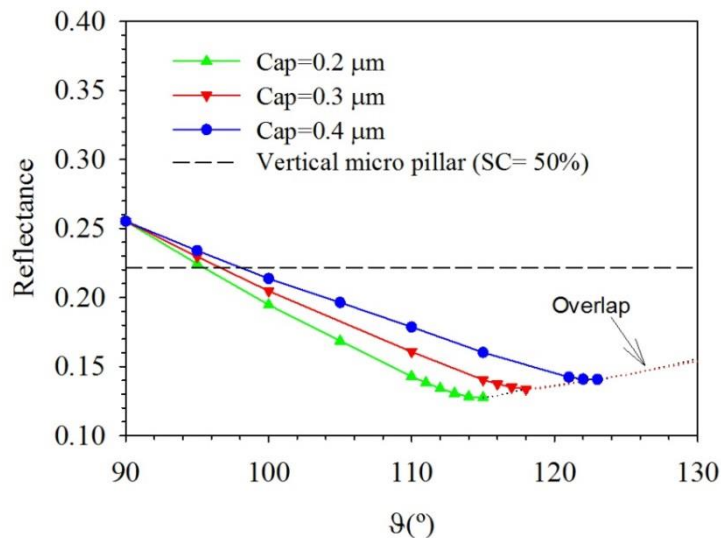


Fig. 6. Reflectance vs θ at $SC=30\%$ varying Cap size for $H=1 \mu\text{m}$.

The Cap in the pattern determines the length of the vertical element in the structure. Figure 6 shows R for different Cap thicknesses while keeping SC constant at 30% and $H=1 \mu\text{m}$. We include results for vertical micro pillar of similar H .

As we increase Cap, while keeping ϑ constant, there is an increase in R. This is because the hut has a bigger vertical component and more of the incoming light hits this portion at larger angle of incidence, leading to an increase in R. Therefore, in order to have a good performance a lower value of Cap is better.

We have shown the impact of each of the structural parameters on R. The number of parameters is large and there is a complex inter-play between them. Therefore, it can be difficult to appreciate how best to choose an optimal set of ϑ , H, Cap and SC values. We present in the next section a study on optimum set of parameters.

4.4 Identifying an optimum set of parameters

Figure 7 displays R as a function of ϑ , SC and Cap. We record the ϑ value giving the lowest R for different SC and H values. Then, we plot it against its corresponding R value. The different symbols and colours stand for different H and SC respectively.

It is possible to see from Fig. 7 the optimum value of ϑ reducing as SC increases. Further to this, for all SC the difference in the optimum ϑ between different heights reduces as H increases. This is in line with our discussion in section 4.2. Moreover, for any given height, the optimum ϑ reduces as SC increases. This is in line with our discussion on section 4.1. A useful insight, for fabrication, is the flexibility of the pattern to achieve optimisation for a given H and Cap. It can be achieved by finding the optimum ϑ for a specific SC that can be fabricated or by finding the optimum SC for a given ϑ that can be etched.

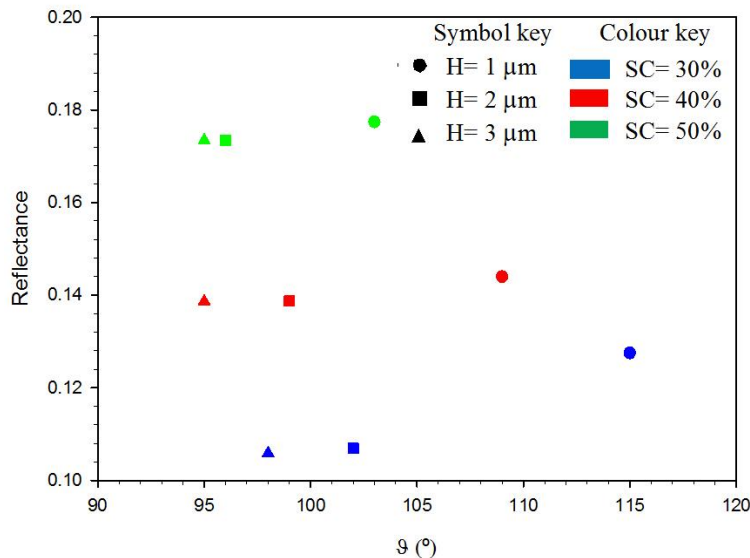


Fig. 7. Reflectance vs Optimum ϑ for different values of H and SC with Cap = 0.2 μm .

5. Conclusions

We have investigated a new hut-like texturing pattern with excellent Reflectance performance and have analysed its critical parameters. The optimal performance of the hut like pattern offers lower Reflectance than nanowires and pyramids for shorter and longer

wavelength ranges respectively. The biggest advantage of hut-like is more efficient light trapping. Furthermore, it enables patterns with low SC to have an excellent performance when θ is optimized. It offers the possibility of low surface recombination.

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Figure captions

Fig. 1. Schematic of proposed hut-like micro pillar array.

Fig. 2. Performance comparison of hut-like structure with other texturing patterns.

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