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# Journal of Biomedical Optics

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## **Photoplethysmographic measurements from the esophagus using a new fiber-optic reflectance sensor**

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# Photoplethysmographic measurements from the esophagus using a new fiber-optic reflectance sensor

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**Abstract.** A prototype fiber-optic reflectance-mode pulse oximetry sensor and measurement system is developed for the purposes of estimating arterial oxygen saturation in the esophagus. A dedicated probe containing miniature right-angled glass prisms coupled to light sources and a photodetector by means of optical fibers is designed and used to record photoplethysmographic (PPG) signals from the esophageal epithelium in anesthetized patients. The probe is inserted simply by an anesthesiologist in all cases, and signals are recorded successfully in all but one of 20 subjects, demonstrating that esophageal PPG signals can be reliably obtained. The mean value of the oxygen saturation recorded from the esophagus for all subjects is  $94.0 \pm 4.0\%$ . These results demonstrate that  $SpO_2$  may be estimated in the esophagus using a fiber-optic probe. © 2011 Society of Photo-Optical Instrumentation Engineers (SPIE). [DOI: 10.1117/1.3598858]

Keywords: pulse oximetry; esophagus; fiberoptic; photoplethysmography; oxygen saturation.

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## 1 Introduction

Pulse oximeters are reported to fail in patients with compromised peripheral perfusion.<sup>1,2</sup> Pulse oximetry is a pulse-dependent technique, and any significant reduction in the amplitude of the pulsatile component of the photoplethysmographic (PPG) signal can lead to inaccuracies in the reported blood oxygen saturation ( $SpO_2$ ) values.<sup>3</sup> When peripheral perfusion is poor, as in states of hypovolemia, hypothermia, and vasoconstriction, oxygenation readings have been shown to become unreliable or, in severe cases, cease completely.<sup>4-6</sup> In a retrospective study where 9203 computerized anesthesia records were reviewed, gaps in pulse oximetry data of at least 10 min were reported in 9.18% of cases.<sup>7</sup> Developments in pulse oximetry technology, in particular, Masimo signal extraction technology (SET) have demonstrated improved performance in low-perfusion states.<sup>8</sup> However, in the complete absence of any peripheral pulse, or in patients with severe burns or other external injuries, peripheral probes would be inapplicable.

To overcome the problems associated with the measurement of  $SpO_2$  at peripheral sites, an optical fiber-based oximetry system was designed for estimating the oxygen saturation ( $SpO_2$ ) in internal tissue from photoplethysmographic signals obtained using red and infrared light sources. The esophagus was chosen as a suitable internal measurement site because it is well supplied with arterial blood and its internal surface is readily accessible in anesthetized patients. Kyriacou *et al.* previously described a non-fiber-optic esophageal pulse oximetry system.<sup>9</sup> A reflectance-mode esophageal probe comprising two infrared and two red light-emitting diodes [(LEDs), of peak emission

880 and 655 nm, respectively] arranged adjacent to a photodetector was designed to fit into a size 20 French gauge plastic transparent disposable stomach/esophageal tube.<sup>10</sup>

An initial clinical study was performed in healthy patients undergoing general anesthesia requiring tracheal intubation. After induction of anesthesia, the probe was placed into the esophagus until the end of the probe was between 25 and 30 cm from the upper incisors. A finger probe containing an identical arrangement of optoelectronic components was placed on the finger for comparison. It was found that the amplitudes of the esophageal PPGs were on average approximately three times larger than those obtained simultaneously from a finger for both wavelengths.

A follow-up clinical study<sup>11,12</sup> investigated and compared esophageal and finger PPG signals and  $SpO_2$  in 49 patients undergoing hypothermic cardiopulmonary bypass surgery. Photoplethysmographic signals were observed at various depths in the esophagus and esophageal  $SpO_2$  values were compared to those measured using a commercial finger pulse oximeter. Measurable PPG traces at red and infrared wavelengths were obtained in the esophagus in all 49 patients.<sup>11</sup> The bias (commercial pulse oximeter minus esophageal pulse oximeter) was  $-0.3\%$  and the standard deviation was  $1.5\%$ . Of the 49 patients included in the study, it was found that five patients had one or more periods of at least ten consecutive minutes, during which the commercial finger pulse oximeter failed to display PPG signals and  $SpO_2$  values, despite being correctly positioned on the finger. Conversely, the esophageal pulse oximeter operated successfully throughout these periods. Use of the esophageal pulse oximeter has also been successfully demonstrated in patients suffering from major burns.<sup>13</sup> Another study using a smaller version of the esophageal pulse oximetry probe showed that reliable signals could be obtained from neonatal and paediatric patients.<sup>14</sup>

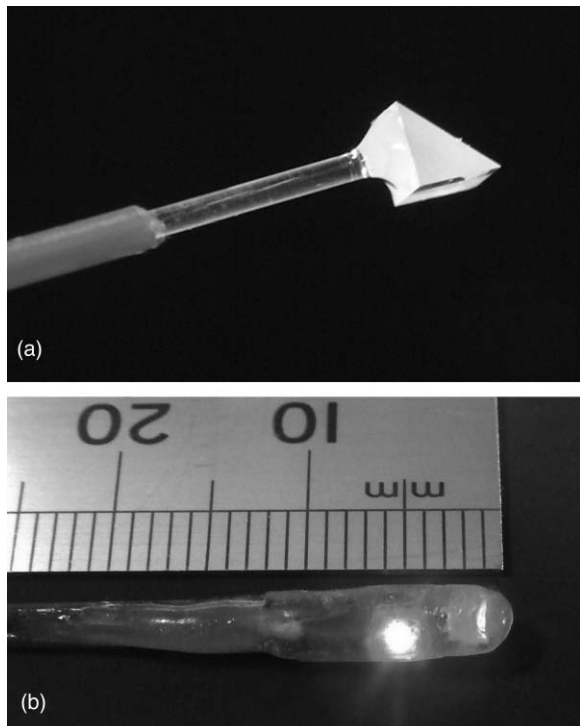
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Although the non-fiber-optic probe performed satisfactorily, the use of an optical fiber-based probe was suggested because the use of fibers confers several benefits and advantages. As well as permitting miniaturization of the probe, silica glass optical fibers are inert and thus are inherently biocompatible and sterilizable. In addition, the fibers are insulators; thus, the patient is electrically and thermally isolated from the optoelectronic components that are confined to the instrumentation unit. The use of optical fibers for tissue illumination and to transmit photoplethysmographic signals from tissue has been demonstrated in clinical applications, notably in pulse oximeters used in magnetic resonance imaging scanners.<sup>15</sup> In the research domain, fiber-optic photoplethysmographic probes have been used for cerebral oximetry,<sup>16,17</sup> spinal cord perfusion monitoring,<sup>18</sup> and intraoperative assessment of splanchnic perfusion.<sup>19</sup>

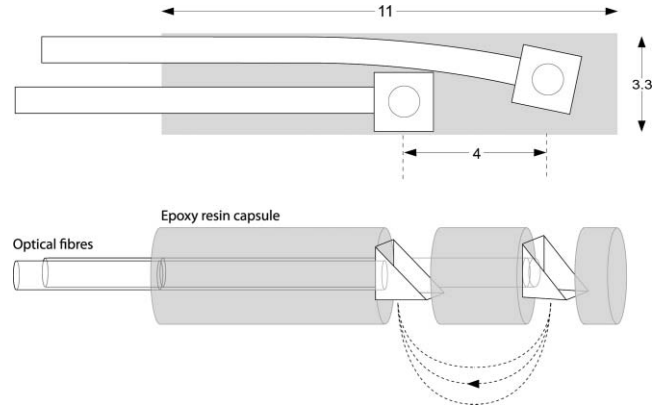
## 2 Methods

### 2.1 Fiber-Optic Sensor

In the present study, a fiber-optic sensor for use in the esophagus<sup>20</sup> was designed and evaluated in 20 patients undergoing surgery requiring tracheal intubation and mechanical ventilation. The esophageal sensor contains a pair of fibers, each coupled to a prism that has the function of changing the path of the light through an angle of 90 deg. The light is thus transmitted and received in a direction perpendicular to the axis of the fiber, unlike a bare fiber, which transmits and receives light in a cone whose axis is aligned with the cylindrical axis of the fiber. Once in position within the esophageal lumen, the probe illuminates the mucosal wall of the esophagus along an axis



**Fig. 1** Photographs of (a) a prism attached to an optical fiber prior to fabrication of the esophageal probe and (b) the finished probe.

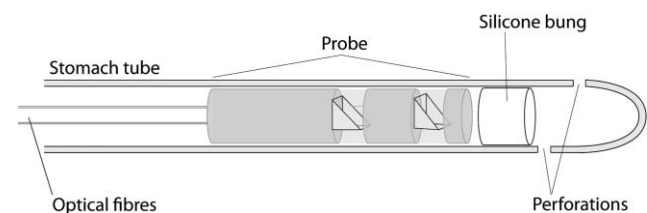


**Fig. 2** Simplified diagram of the fiber-optic esophageal oximetry probe. Approximate dimensions shown in millimeters.

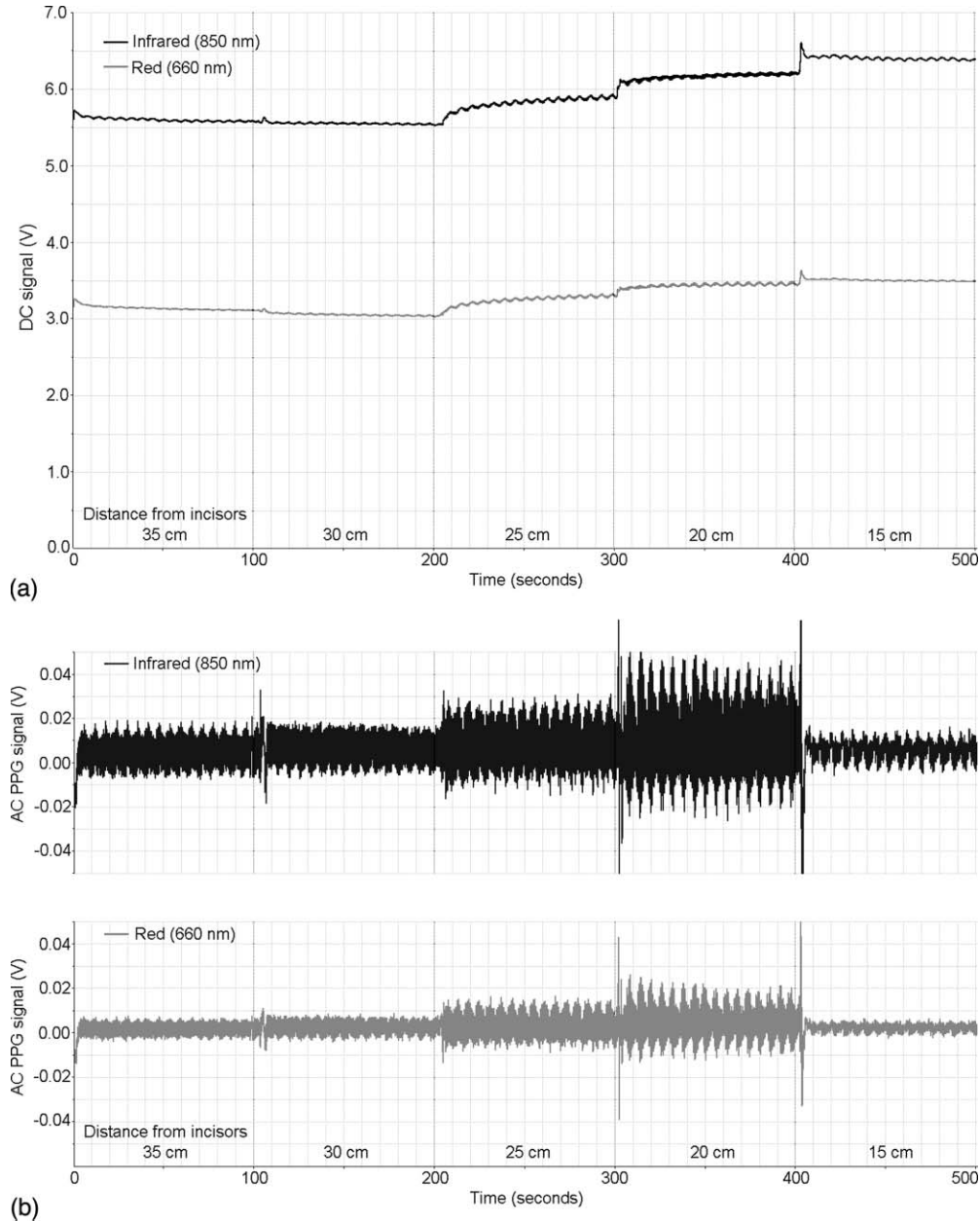
normal to the wall of the esophagus, and is similarly sensitive to light backscattered normally from the esophageal wall.

The esophageal probe was constructed from a pair of optical fibers each with a core diameter of 600  $\mu\text{m}$ . The distal ends were polished flat using grade 5 followed by grade 3 sandpaper. A right-angled triangular glass prism (Edmund Optics, York, United Kingdom) of dimensions  $2 \times 2 \times 2$  mm was affixed to the ends of each optical fiber using 144-M glass adhesive (Dymax Inc., Torrington, Connecticut), as shown in Fig. 1(a). The reflecting face (the hypotenuse face) of each prism was covered with OP-19 optical blocking adhesive (Dymax Inc.) and the fibers, with the prisms attached, were placed in a hemicylindrical mold. A two-part biomedically compatible epoxy resin was then injected into the mold and left to set. The blocking adhesive was then removed, and successive layers of epoxy were added taking care to keep the reflecting surfaces of the prisms free of epoxy, which was achievable by injecting the liquid epoxy using a syringe and needle. The viscosity of the epoxy prevented it from flowing onto the outer reflecting face of each prism. Each layer of epoxy was allowed to set until the probe was almost cylindrical in shape. The probe was filed with emery board until almost perfectly cylindrical as shown in Fig. 1(b). A diagram of the finished probe is shown in Fig. 2.

The probe was designed for insertion into a size 18 French gauge stomach feeding tube. The stomach tube keeps the probe isolated from body fluids; thus, the probe may be reused with a new tube without the risk of cross-contamination between patients. The stomach tube has two perforations close to the distal end that were blocked using a silicone bung inserted through one of the perforations and advanced proximally prior to use (see Fig. 3). The tube was also marked using a nontoxic sterile



**Fig. 3** Esophageal probe inserted into a size 18 French gauge stomach feeding tube.



**Fig. 4** Example of a 100-s recording of the dc (a) and normalized ac PPG (b) infrared and red signals at all five measurement depths for one patient (patient number = 17).

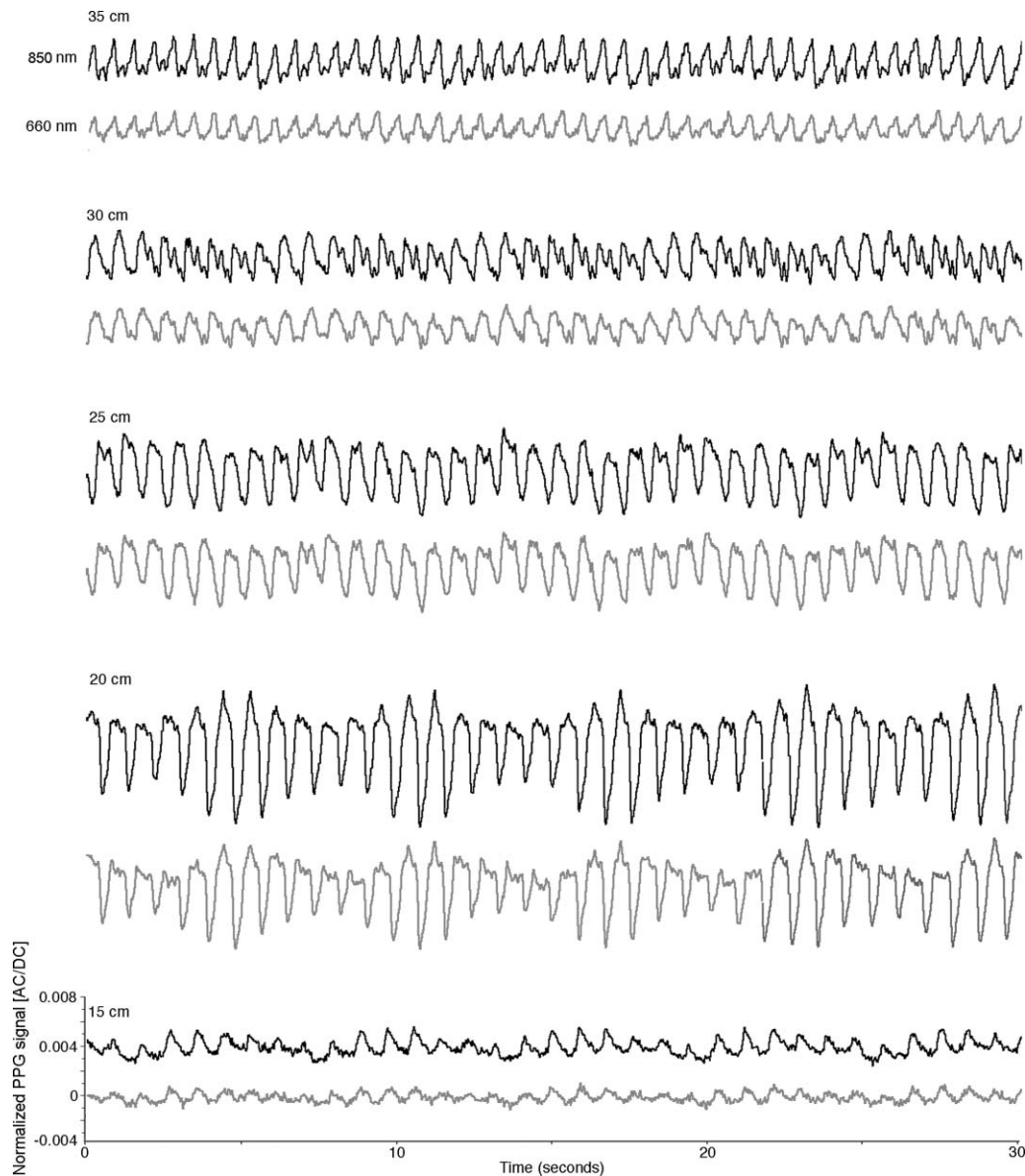
permanent marker at 5-cm intervals to enable accurate positioning in the esophagus. As a further precaution, the probe itself was decontaminated in a 70% propan-2-ol solution between patients.

## 2.2 Data Acquisition System

The data acquisition system for this study<sup>17</sup> has been developed and evaluated in our laboratory and is based on a fiberoptic probe comprising two optical fibers, one of which is used to transmit light to the tissue and the other to return a fraction of the backscattered light to a photodetector. A signal processing system consisting of a circuit interfaced with a notebook computer has been implemented for calculation of clinical vari-

ables from the measured light intensities and is subsequently described.

The light sources used are red and infrared LEDs mounted in Sub Miniature A (SMA) packages (Optoelectronic Manufacturing Corporation Ltd., Redruth, United Kingdom). The infrared LED used for the short-duration measurements has a peak emission wavelength of 850 nm, whereas the device used for the long-duration measurement has a peak emission at 940 nm. The red LED used for both studies has a peak emission wavelength of 660 nm. Both LEDs are connected to the single transmitting optical fiber using a Y-coupler, i.e., a bifurcated optical fiber assembly (Ocean Optics Inc., Dunedin, Florida). The photodetector is an SMA-packaged positive intrinsic-negative (PIN) photodiode of active surface area 0.8 mm<sup>2</sup> (Optoelectronic Manufacturing



**Fig. 5** Thirty-second samples of the normalized ac PPG waveforms obtained at each measurement depth. The waveforms were obtained from the same data set shown in Fig. 4. All traces are plotted on the same vertical scale.

Corporation Ltd.). The photodetector is coupled directly to the receiving optical fiber.

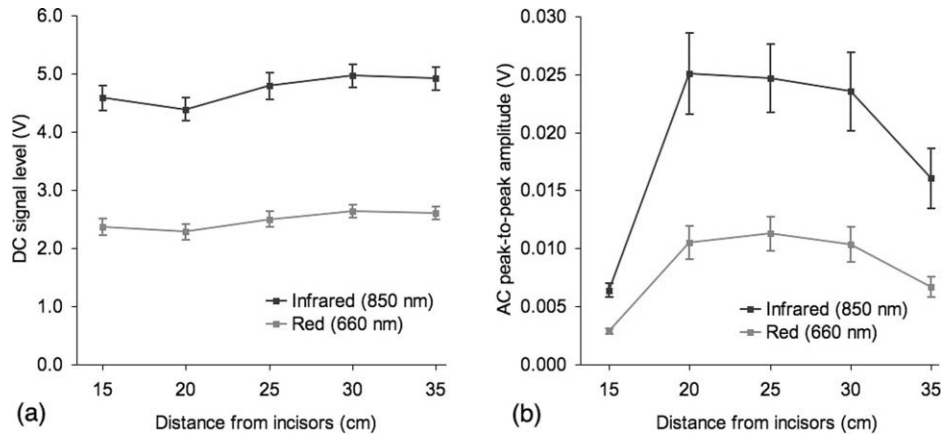
An instrumentation unit is used for the control of the light sources and acquisition of signals from the tissue. This hardware is interfaced to a 16-bit DAQCard-AI-16XE-50 data acquisition card (National Instruments Inc., Austin, Texas) installed into a notebook computer. The LEDs are driven by a pair of switchable regulated current sources, one for each wavelength, supplying 25 and 14 mA to the red and infrared LEDs, respectively. Timing signals are provided by a programmable counter and timer built into the data acquisition card.

The photodiode is connected to a differential transimpedance amplifier. The output of the transimpedance amplifier is fed into a demultiplexer, and the signals are separated into three components, representing the infrared and red light intensities. The total intensities of the red and infrared signals are obtained by filtering to remove high-frequency switching noise from the

demultiplexer using second-order low-pass Butterworth filters, each with a cutoff frequency of 16 Hz (at  $-3$  dB). A further high-pass filter stage with a cutoff frequency of 0.4 Hz is incorporated into each channel to separate the PPG (or ac) signal from the total (ac + dc) signal. The instrumentation is powered by two 12-V 1.2-Ah sealed lead-acid batteries (Yuasa Battery Inc., Laureldale, Pennsylvania). The signals are all fed into the analog-to-digital converter built into the data acquisition card installed in the notebook computer running a LabVIEW (National Instruments Inc., Austin, Texas) Virtual Instrument (VI). The VI reads the digitized signals at a rate of 100 samples per second and records the signals in a spreadsheet file.

### 2.3 Patient Measurements

The study was approved by the local Independent Ethics Committee and permission was given to conduct the study in 20



**Fig. 6** Graphs showing mean ( $\pm$  SEM) dc signal levels (a) and the unnormalized mean ( $\pm$  SEM) peak-to-peak amplitudes of the ac PPG signals (b) plotted against depth in the esophagus for all 19 patients.

patients. The instrumentation was also approved for safety by the Medical and Healthcare Products Regulatory Agency (MHRA). Patients undergoing minor general surgical procedures requiring tracheal intubation and ventilation were deemed suitable for this study. Adult patients aged (18–70) and deemed “low risk” by the American Society of Anesthesiologists (score of 1–3) were identified from the elective operating lists at Barts and The London NHS trust. Any patients with esophageal pathologies, or those in whom difficulty or increased risk of probe placement was anticipated, were excluded.

After induction of anesthesia and immediately after tracheal intubation, the probe contained within a sterile stomach tube was inserted into the esophagus by the anesthetist, via the patient’s mouth, under direct vision with a laryngoscope. The tip of the probe was placed at a depth of 35 cm in the esophagus as measured from the front incisors. Once the probe was in position, the light sources were switched on and signals recorded for 100 s. A 100-s measurement period was chosen to allow sufficient data collection without unnecessarily prolonging the patient’s anesthesia. The probe was then withdrawn 5 cm at a

time and signals were recorded for a further 100 s at each position until the probe was at a depth of 15 cm. The arterial oxygen saturation was measured using a commercial finger pulse oximeter (Datex-Ohmeda, Helsinki, Finland). The probe was removed at the end of the measurement period, before the patient was moved from the anesthetic room to the operating theater, and surgery commenced. Each patient was reviewed, postoperatively, to check for any adverse events.

## 2.4 Signal Processing

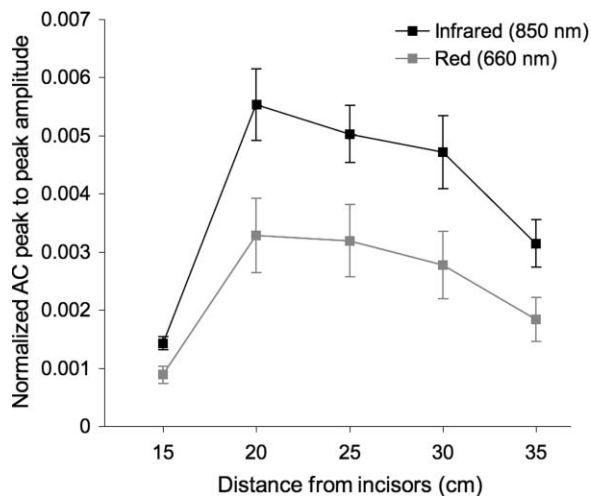
The ac PPG signals were normalized by dividing the signal by the simultaneously recorded ac + dc signals. The peak-to-peak amplitudes of the normalized PPG signals were calculated for each heartbeat using a peak-and-valley detection algorithm incorporated into a LabVIEW virtual instrument. The mean value of  $R_R$  for each data stream (100 s) for each wavelength thus,

$$R_R = \frac{\left( \sum_{i=1}^n A_{i,R} \right) / n}{\left( \sum_{i=1}^n A_{i,IR} \right) / n} \quad (1)$$

where the  $A_{i,R}$  and  $A_{i,IR}$  are the peak-to-peak amplitudes of the  $i$ ’th red and infrared normalized PPG cycle in the data streams, respectively, and  $n$  is the total number of PPG cycles (heartbeats) in the data stream. The ratio of ratios  $R_R$  was thus averaged over a 100-s time period. The mean value of  $R_R$  was used to estimate the arterial oxygen saturation ( $SpO_2$ ) by substituting in

$$SpO_2 = 110 - 25R_R \quad (2)$$

which is a linear approximation to an empirically determined calibration curve, obtained from measurements in healthy volunteers.<sup>21</sup> It should be noted that this equation was derived using a measurement system utilizing a 940-nm infrared light source. The instrumentation incorporated an 850-nm LED for the short-duration study; thus, some error in estimation was expected. However, because no other equation was available, Eq. (2) was used to produce an approximate estimation of oxygen saturation.



**Fig. 7** Graph showing normalized mean ( $\pm$  SEM) peak-to-peak amplitude of ac red and infrared PPG signals measured from the esophagus in 19 patients.



### 3 Results

Signals were obtained successfully from 19 patients, with one failure attributable to a technical fault. Examples of the dc and ac signals recorded at all five measurement depths for a typical patient are shown in Fig. 4. These signals represent a continuously recorded data stream. The probe was repositioned within a few seconds between measurements, by simply withdrawing it by 5 cm at the mouth, causing minimal interference to the traces.

It can be seen from Fig. 4(a) that moving the probe to each monitoring position caused a small change in dc signal level. Furthermore, in some cases there was a small “settling-in” time during which the signal level changed slowly. In the example shown, there was significant drift in the signal during the entire time the probe was at the 25-cm position. The dc signal also exhibited a small amount of periodic modulation occurring at the respiratory frequency. Figure 4(b) shows that the amplitude of the ac PPG signal varied considerably with measurement depth, and there was also respiratory modulation present in this signal. Note that the dc and ac PPG waveforms have been compressed horizontally so little detail can be discerned in either case.

Figure 5 shows 30-s samples of the waveforms obtained at each depth for the same patient. The waveforms in this plot were also normalized by dividing the ac signal by the simultaneously recorded dc signal. In all cases, the most significant periodic feature occurred at a frequency consistent with the cardiac frequency, but the waveform also contained a low-frequency modulation at  $\sim 0.18$  Hz, equal to the frequency of artificial ventilation. This modulation affected the position of the peaks and “valleys” (i.e., the waveform’s peak-to-peak amplitude) and the position of the “baseline” was also modulated. It can be seen that the morphology of the PPG waveform varied considerably with the depth of measurement. As well as the change in amplitude with depth, the ventilator modulation varied in amplitude relative to the periodic cardiac variation. Between 35 and 25 cm, for example, there was significant baseline modulation but at depths of 20 cm or less, modulation of the peak-to-peak amplitude appeared to dominate the signal.

Figure 6 shows graphs of the mean dc signal levels and mean ac PPG peak-to-peak amplitudes of the signals calculated over the 100-s measurement periods for all 19 patients. The average dc signal level was calculated for each depth for each patient, and the mean ( $\pm$  SEM) values were calculated for all patients. The average un-normalized ac signal amplitudes were calculated for each depth and each patient, and again the mean ( $\pm$  SEM) values calculated for all 19 patients. It can be seen that the dc signals showed a slight trend of increasing signal level with increasing depth, although the differences in signal levels between depths were not statistically significant. As with the individual example shown in Figs. 4 and 5, the mean ac signal amplitudes showed considerable variation with depth. Specifically, the ac signals recorded from the mid to lower esophagus (depths of 20 cm or greater) had considerably larger mean amplitudes at both wavelengths than those in the upper esophagus (15 cm).

Figure 7 shows a graph of the mean ( $\pm$  SEM) of the normalized ac PPG amplitudes at red and infrared wavelengths at the five monitoring depths. The signals were normalized by dividing the ac signal by the simultaneously recorded dc signal

level before calculating the mean values. Such normalized ac PPG amplitudes may be used in Eq. (1) to calculate the ratio of ratios ( $R_R$ ). The maximum mean esophageal amplitude for both wavelengths occurred at the depth of 20 cm. The amplitudes of the red and infrared normalized PPG signals obtained at 15 cm were significantly smaller ( $P < 0.001$ ) than those obtained at all other depths, as evaluated by a paired Student’s *t*-test. There was no significant difference between amplitudes at other adjacent depths (i.e., 20–25, 25–30, and 30–35 cm).

The mean ratio of ratios for each patient, at each measurement depth was calculated from the normalized PPG amplitudes, using Eq. (1) and the estimated oxygen saturation calculated using Eq. (2). The estimated oxygen saturations obtained from each depth are presented in Table 1. In some cases, it was not possible to calculate the ratio of ratios because the signal quality was very poor. It can be seen that there is considerable

**Table 1** Arterial oxygen saturation SpO<sub>2</sub> derived from PPG signals obtained at all five depths in the esophagus for each patient.

Patient #	SpO <sub>2</sub> estimated at each esophageal depth (%)					CV%
	15 cm	20 cm	25 cm	30 cm	35 cm	
1	*	93.9	91.1	90.9	85.5	3.89
2	*	92.7	93.6	92.2	*	0.76
3	97.6	92.9	97.4	100.6	103.2	3.93
4	96.2	98.0	84.0	79.1	77.2	11.1
5	*	90.0	93.4	96.7	101.1	4.97
6	*	95.1	100.0	89.9	*	5.32
7	*	94.4	94.2	100.0	84.4	6.95
8	87.4	93.3	91.5	88.3	99.5	5.24
9	95.1	95.6	96.7	88.7	98.1	3.82
10	89.3	91.9	91.7	94.1	93.9	2.12
11	77.3	90.2	87.0	95.2	92.7	7.85
12	98.3	91.9	94.7	93.5	91.9	2.81
13	79.4	92.4	92.0	98.0	92.9	7.58
14	94.4	92.7	96.4	94.5	69.4	12.6
15	*	89.9	93.6	89.3	92.2	2.20
16	91.5	92.5	96.5	83.8	97.4	5.85
17	94.8	93.7	89.4	93.0	94.6	2.35
18	95.9	94.0	90.9	95.8	97.4	2.63
19	88.8	91.4	89.0	95.7	97.0	4.11
CV%	7.31	2.16	4.17	5.76	9.49	

\*No value could be calculated due to poor signal quality.

**Table 2** Mean heart rate, mean normalized peak-to-peak amplitudes, mean ratio-of-ratios and SpO<sub>2</sub> derived from PPG signals obtained at the best depth in the esophagus for each patient. Finger SpO<sub>2</sub> values from a commercial pulse oximeter are also shown. Note that the best depth giving the maximum esophageal PPG signals varied from patient to patient and was usually between 20 and 30 cm.

Patient No.	"Best" depth (cm)	Mean heart rate (min <sup>-1</sup> )	Normalized PPG amplitudes		Mean ratio-of-ratios	Mean esoph. SpO <sub>2</sub> (%)	Finger SpO <sub>2</sub> (%)
			Red (/10 <sup>-3</sup> )	Infrared (/10 <sup>-3</sup> )			
1	30	65.6	10.7	14.0	0.76	90.9	99
2	20	72.5	11.6	16.8	0.69	92.7	99
3	30	92.4	1.03	2.74	0.38	100.6	100
4	25	63.2	7.14	6.86	1.04	84.0	99
5	25	64.5	16.5	24.8	0.67	93.4	98
6	25	88.1	4.94	12.4	0.40	100.0	100
7	30	81.7	3.72	9.33	0.40	100.0	99
8	25	61.9	4.82	6.52	0.74	91.5	99
9	20	75.0	3.22	5.58	0.58	95.6	99
10	35	88.6	2.68	4.16	0.64	93.9	99
11	30	76.8	4.85	8.21	0.59	95.2	98
12	35	68.4	3.98	5.51	0.72	91.9	99
13	30	77.9	3.73	7.80	0.48	98.0	100
14	30	77.1	4.14	6.68	0.62	94.5	99
15	25	77.1	2.57	3.91	0.66	93.6	100
16	25	85.5	3.66	6.78	0.54	96.5	100
17	20	71.4	5.59	8.59	0.65	93.7	99
18	25	58.9	6.08	7.95	0.76	90.9	99
19	25	60.6	1.67	1.99	0.84	89.0	100

variation both in the estimated oxygen saturation between patients and, in many cases, between depths for a particular patient.

To compare the signals between patients, a "best" depth was chosen for each patient (i.e., the depth at which the infrared PPG amplitude was greatest). This depth was found by manual measurement of the amplitudes from printouts of the PPG waveforms. Table 2 summarizes several variables derived from the signals for each patient obtained at the best depth. It can be seen that, even if the largest PPG amplitudes obtained for each patient are compared, there is considerable variability in the values of the amplitudes. The mean value ( $\pm$  SD) of the best depth oxygen saturation for all patients was 94.0% ( $\pm$  4.0%), while the mean ( $\pm$  SD) oxygen saturation recorded from the finger with the commercial pulse oximeter was 99.2% ( $\pm$  0.6%). The bias between the two measurements (esophageal and finger) was thus -5.2%.

#### 4 Conclusion

This study demonstrated that reliable photoplethysmographic signals may be obtained from the esophageal wall using a fiberoptic probe. The acquired PPG signals showed different morphology at different depths, and in particular, the mean AC amplitude varied depending on the depth of the monitoring site. This is likely due to variability in vessel distribution at different locations in the esophagus. The degree of respiratory modulation of the signals also showed significant variation with depth. Although there was a change in the mean dc signal level for all patients at different monitoring depths [as shown in Fig. 4(a)], Figs. 4(b) and 5 show that the variation in the normalized PPG signal amplitudes was mostly caused by variations in ac PPG amplitude at different monitoring depths. The measurements suggest that the greatest amplitude signals, and therefore, probably the most suitable measuring site is 20–30 cm from the teeth. The amplitudes of both the red and infrared normalized

PPG signals at 15 cm were significantly smaller than those at all other depths. These findings were similar to those of Kyriacou et al., who compared PPG signals at the same depths with their non-fiber-optic probe, except that, in the case of the red wavelength, they found no significant difference between the amplitudes at depths of 15 and 35 cm.<sup>11</sup>

The oxygen saturations estimated at all depths showed that there was large variation in values between patients and between depths for many patients. At some depths, the signal quality was poor; thus, a saturation value could not be produced. A best depth value was therefore chosen for each patient. The mean value of the best depth oxygen saturation was  $94 \pm 4.0\%$ , 5.2% lower than that recorded from the finger using the commercial pulse oximeter. The negative bias may be attributable to the use of an algorithm [Eq. (2)] for calculation of the SpO<sub>2</sub>, which was developed from experimental measurements using transmittance mode probes on a different measurement site (the finger rather than the esophagus). Kyriacou et al. found their esophageal measurements to be, on average, 6.5% lower than those measured from a commercial finger pulse oximeter.<sup>9</sup>

Another possible source of inaccuracy is the mechanical artefact induced by the patient's heartbeat and ventilation due to the proximity of the probe to the heart and lungs. It has been observed that the PPG signals are sensitive to movement of the fiber tips relative to the tissue surface as well as to movement of the fibers themselves. Periodic (ac) modulation could be induced in the detected signals with cardiac and/or respiratory frequency components. The respiratory frequency modulation was observed in the signals (see Figs. 4 and 5), whereas cardiac frequency modulation would be impossible to distinguish from the "real" PPG. It may be supposed that this induced movement modulation would be similar in magnitude for both wavelengths. This would result in the calculated ratio of ratios being higher than in the case with no movement because, in a hypothetical situation of movement present, with no PPG, the ratio of ratios would be equal to 1. The oxygen saturation would be underestimated, (because, for arterial blood, the ratio is normally <1).

This study aimed to investigate whether PPG signals could be obtained from internal vascularized tissue using a fiber-optic probe. Other than by commercial pulse oximetry (which is not considered a gold standard method), accurate measurements of the arterial oxygen saturations were not recorded; thus, further analysis of oxygen saturation in these patients was not deemed appropriate for this pilot study. The purpose of this study was merely to demonstrate that signals could be acquired in the majority of patients and that the oxygen saturation values derived from an approximate algorithm were in the expected range we might expect in this patient population under experimental conditions. These esophageal measurements demonstrated that PPG signals may be reliably obtained from internal tissue using a reflectance mode fiber-optic probe. A controlled study in a greater number of patients is planned, where readings from the esophageal pulse oximeter will be compared to CO-oximetry arterial blood samples. Esophageal Doppler blood flow will also be recorded. A separate animal study is also planned, where esophageal saturation will be recorded during induced hypoxemia. The data from these studies should allow a new esophagus-specific algorithm for calculation of oxygen saturation from the esophageal signals.

This study, as well as previous studies by Kyriacou et al.,<sup>9–12,14</sup> have demonstrated that the esophagus has potential as an alternative monitoring site for pulse oximetry. The finger and earlobe will almost certainly remain the location of choice for pulse oximetry measurement in almost all cases, by virtue of the ease of access and noninvasiveness of these sites. Furthermore, there is a very small possibility of gastroesophageal injury, such as esophageal tear associated with placement of esophageal probes, whereas the risk of injury from a finger probe is negligible. In certain clinical situations, such as extremely low-perfusion states where even SET-type pulse oximeters fail, or in patients in whom such sites are not available, the esophagus could provide a viable option because the central organs are preferentially perfused. A disposable fiber-optic probe similar to that described in this paper could perhaps be incorporated into gastric feeding tubes or similar medical equipment used in the intensive care unit (ICU). Such a device could also find application in neonates or small infants who are unwilling to tolerate a finger probe.

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