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Progressive Collapse Analysis of Reticulated Shell structure under Severe Earthquake considering the Damage Accumulation Effect

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Abstract:

A reticulated shell is one of the conventional long span space structures, prone to progressive collapse under a severe earthquake due to its unique single layer feature.

This is. However, the collapse mechanism of this type of structure is not well studied. In this paper, a numerical modelling technique using the fiber beam elements is developed. The correspondent material model based on the inclusion of damage accumulation was also developed in order to determine the failure criteria of structural members. An effective way to simulate the buckling behavior of the structural members is also used in the numerical simulation. The relevant numerical method is developed and validated against experimental tests: good agreement is achieved. Based on this numerical method, a parametric study of the reticulated shell under severe earthquake loading is performed and the responses of the structure is investigated and a three-stages collapse mechanism of this type of structure was observed.

Key words: single-layer reticulated shell; progressive collapse; severe earthquake, cumulative damage; hysteresis curve; stiffness degradation

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20 **Introduction**

21 The event of the 9/11 in 2001 embarked the research on the causes of progressive collapse in
22 structures and possible mitigating methods. Increasing attention has been paid on the studies of
23 collapse mechanism and collapse prevention methods of buildings in recent years. However, few
24 studies have been performed toward the collapse mechanism and relevant collapse prevention
25 measures for space structures. For a single layer space structures, such as the reticulated shell,
26 stability is pressing important, as this type of structure is prone to local buckling which may initiate
27 the dynamic global buckling and collapse of the entire structure under the severe earthquake.
28 Therefore, the research in this area is imperative.

29

30 There are some design procedures in Europe and U.S. available on mitigating the progressive
31 collapse of buildings, such as design guidance of the Department of Defense (DoD) (2005) and the
32 General Services Administration (GSA) (2003) ASCE 7 (2010) in U.S; the design code of British
33 Building Regulations (2004), BS5950 (2001) in U.K. Some references such as FEMA 2002 (2002)
34 and NIST 2005 (2005) also provide general design recommendations, which require steel-framed
35 structural systems to have enough redundancy and resilience. However, most of these design codes
36 are focused on buildings; no detailed design procedure in preventing progressive collapse of
37 reticulated shell is available.

38

39 So far, some numerical investigation (McGuiew,1974),(Powell,2004) and experimental tests
40 Shimada et al. (2008), Tsitos (2008) have been done on the building structures. Starossek, 2009,
41 gave detailed introduction on the collapse mechanisms for different type of structures. Starossek,

42 2006, suggested a pragmatic approach for designing against progressive collapse. Brunesi et al.
43 (2015) developed the fiber-based models for progressive collapse assessment. They integrate the
44 incremental dynamic analysis with the Monte Carlo simulation and developed the fragility
45 functions.

46
47 However, majority of existing research is based on the building structures, little has been noticed on
48 the space structures. See, et al. (1986), discussed the large displacement elastic buckling of the
49 space structures, however, they did not further investigate the collapse mechanism of the whole
50 space structure. Deshpande (2001), discussed the collapse of the truss core sandwich beams.
51 Orbison, et al., 1982 developed an efficient procedure for modelling the inelastic behavior of three-
52 dimensional beam-column. Long,H.V et al. (2008), developed an efficient algorithm for both limit
53 and shakedown analysis of 3-D steel frames by the kinematic method using linear programming
54 technique. Ferrari et al. 2016, developed an innovative formulation of a FEM computational model
55 for the analysis of elastoplastic 3D truss-frame structures. SHEKASTEHBAND et al., 2014
56 discussed the dynamic propagation of the snap-through buckling in Tensegrity structures.
57 Blandford(1996) performed progressive analysis of inelastic space truss structures. Kato et al. (1998)
58 discussed the collapse of semi-rigidly reticulated domes with initial geometric imperfections.
59 Malla(2011) proposed the methodology suitable for the dynamic analysis of the progressive failure
60 of truss structures. Fang et al. (2001) performed the simulation of the progressive collapse together
61 with a study of suitable methods for resisting progressive collapse of single layer grid structures
62 based on ANSYS and LS-DYNA.

63 In above research, damage accumulation is ignored in most of the numerical models. However, in

64 the event of earthquake, damage accumulation can be resulted by the cyclic loading during
65 earthquake. Therefore, when investigating the dynamic response of structure under earthquake
66 loading, damage accumulation is essential to accurate prediction of dynamical response of
67 structures in numerical simulation. However, little work has been done in this area.

68

69 Therefore, in this paper, based on thermodynamic theory, the damage evolution equations for fiber
70 beam element is derived. The corresponding constitutive relationship for beam elements are also
71 developed. The relevant numerical analysis method is also developed. In addition, due to the
72 redundancy and indeterminacy of this type of structures, dynamic instability criterion based on
73 implicit algorithm can capture neither the collapse mechanism of the reticulated shell, nor the
74 failure mode of individual components. Therefore, the simulation of the whole collapse process
75 requires application of explicit dynamic algorithm which is used in this paper.

76 Based on above studies, a subroutine program based on explicit dynamic algorithm is developed to
77 analyze the response of the single-layer reticulated shell under severe earthquake. The program was
78 validated against experimental tests. It is validated that, the proposed numerical method can
79 accurately simulate the members failure, the redistribution of internal forces and the collapse
80 mechanism of the whole structure. Based on this numerical method, parametric studies on single
81 layer reticulated shell is performed and the collapse mechanism of this type of structure is studied.

82

83 In this paper, the authors deal with earthquake-induced failure of some members, in most cases,
84 global failure rather than a localized portion of structure can be observed. Therefore, the subject of
85 this research presented in this paper is primarily to investigate the mechanism of progressive

86 collapse rather than disproportionate collapse, which is usually considered as a special type of
87 progressive collapse in which local failure develops causing a final disproportionate extent of
88 damage.

89 **Numerical algorithm development**

90 As it is shown in Figure 1, a 3D full scale model replicating a single layer reticulated shell is set up
91 in ABAQUS, the related numerical method is introduced in this section. The structural members
92 used in the model are Chinese Tubular sections, with yield stress of 235MPa. The Young's modulus
93 is 2.06×10^5 MPa. The Poisson ratio is 0.3.

94

95 *Fiber beam element method*

96 In this research, all the structural members of the reticulated shell are simulated using the beam
97 elements. Each beam element is further discretized into a number of longitudinal fibers across their
98 cross-section with appropriate constitutive model defined to each fiber as it shown in Figure 2
99 which is the cross-section of a beam element with tubular sections. It can be seen that the beam is
100 subdivided into 8 fibers (numbered from 1 to 8) across its cross-section. Each fiber element
101 comprises 2 nodes with three degrees of freedom at each node. The beam element is integrated by
102 these fibers and every section of the fiber represents one Gauss-Lobatto integration (Maerschallck et
103 al. 2006) point. This so called fiber beam element method has been used for simulating the concrete
104 members, (Taucer,1991) It is based on assumptions of small deformation and plane sections remain
105 plane when load is applied. However, its application in steel members is not widely used. The
106 overall section behavior of the beam is therefore determined by integration of the response of these
107 8 fibers. In another word, the constitutive relation of the cross-section of the beam element is

108 derived by integration of the stress-strain relation of all the 8 fibers. Hence, the total response of
 109 each single beamelement under loading along the length can be further derived. The strain in each
 110 fiber is calculated based on the plane section remaining plane assumption. The stress of each fiber
 111 can be worked out from its strain value.

112 This fiber beam element method is used in this research to simulate all the structural members of
 113 the dome using the general-purpose program ABAQUS.

114

115 ***Constitutive model of the fiber and failure criterion for beam elements***

116 In the proposed method, the cumulative damage is included. Based on strain equivalence hypothesis,
 117 the following constitutive models can be established:

118 In the elastic loading or unloading stage:

119
$$\tilde{\boldsymbol{\varepsilon}}^e = \tilde{\boldsymbol{\sigma}} / \mathbf{E} \tag{1}$$

120 In the plastic loading stage, the strain equivalence hypothesis is still valid, it is:

121
$$\boldsymbol{\varepsilon} = \tilde{\boldsymbol{\sigma}} / \mathbf{E}_t = \boldsymbol{\sigma} / \tilde{\mathbf{E}}_t \tag{2}$$

122

123 Where,

124 $\tilde{\boldsymbol{\varepsilon}}^e$ Is elastic strain tensor

125 $\boldsymbol{\varepsilon}$ is strain tensor

126 $\boldsymbol{\sigma}$ is Cauchy stress tensor

127 $\tilde{\boldsymbol{\sigma}} = \boldsymbol{\sigma} / (1 - D)$ is effective Cauchy stress tensor

128 $\tilde{\mathbf{E}} = \mathbf{E} \cdot (1 - D)$ is effective elastic tensor;

129 D is cumulative damage;

130 \tilde{E}_t is tangent modulus.

131 $\tilde{E}_t = E_t \cdot (1 - D)$ is Effective tangent modulus;

132 D is the cumulative damage variable, which is an independent variable, its value increases
133 monotonically in the plastic state. In Zhou (2010), an incremental damage evolution equation of
134 beam element with steel material is derived according damage evolution model by Chow and Wang
135 (1987). It is shown in Equation (3)

$$136 \quad dD = \frac{1 - D}{2\sigma_{11}} d\sigma_{11} \quad (3)$$

137 Where,

138 σ_{11} is axial stress existing in a fiber beam element,

139 Equation (3) is valid in plastic state.

140 Based on above theory, User Material model for the steel members was developed using the
141 subroutine program VUMAT available from general purpose software ABAQUS, whose algorithm
142 is as follows:

143 **In the elastic loading or unloading stage**, the stress evolution equation is:

$$144 \quad \sigma_{new} = \sigma_{new}^{trial} = \sigma_{old} + \tilde{\lambda} trace(\Delta\varepsilon)I + 2\tilde{G}\Delta\varepsilon \quad (4)$$

145 Where σ_{new} is current stress,

146 σ_{new}^{trial} is trial stress,

147 σ_{old} is stress in the last step,

148 $\Delta\varepsilon$ is incremental strain,

149 $trace(\Delta\varepsilon)$ is Volumetric strain increment,

150 I is unit matrix

151 $\tilde{\lambda}$ and \tilde{G} are two different effective lames constants:

$$\begin{aligned}
152 \quad \tilde{\lambda} &= \frac{Ev(1-D)}{(1+\nu)(1-2\nu)}, \\
153 \quad \tilde{G} &= \frac{E(1-D)}{2(1+\nu)} \tag{5}
\end{aligned}$$

154 **In plastic stage, the stress evolution equation is:**

$$155 \quad \sigma_{new} = \sigma_{new}^{trial} - 2\tilde{G}\Delta\gamma Q \tag{6}$$

156 Where, $\Delta\gamma$ is plastic strain increment, with

$$157 \quad \Delta\gamma = \frac{1}{2G(1+\tilde{H}/3G)} \left((\xi_{new} : \xi_{new})^{1/2} - \sqrt{\frac{2}{3}}\sigma_0 \right) \tag{7}$$

158 Q is Current yield surface normal tensor, with

$$159 \quad Q = \sqrt{\frac{3}{2}} \frac{\xi}{\sigma_0} \tag{8}$$

160 And \tilde{H} is effective plastic gradient,

161 σ_0 is yield radius,

162 $\xi_{new} = \sigma_{new}^{trial} - \alpha_{old}$, is difference between current trial stress and back stress with

$$163 \quad \alpha_{new} = \alpha_{old} + \frac{2}{3}\tilde{H}\Delta\gamma Q \tag{9}$$

164 Where α_{old} is the back stress

165 Therefore, the damage variable D accumulatively changes as follows:

$$166 \quad D_{new} = D_{old} + \frac{1-D_{old}}{2\sigma_{11}} d\sigma_{11} \tag{10}$$

167 Where

168 D_{old} is the damage value of material calculated in last sub-step and input at the beginning
169 of current sub-step.

170 D_{new} is updated damage value in current sub-step.

171

172 ***Failure criterion of structural members***

173 The failure criterion of each fiber is determined based on the studies by the authors in (2010).

174 When D_{new} in a fiber develops into certain value D_{limit} , the fiber is determined as failure. Where:

175
$$D_{limit} = 1 - \left(\frac{f_u}{f_y} \right)^{\frac{1}{2}}$$

176 In the designed VUMAT subroutine program, when the failure of one fiber is triggered, the elastic
177 modulus of this fiber will be set as zero

178 automatically. When all the fibers in a beam element fail, that beam element is determined as failure,

179 thus this beam element will be deleted by the program. After an element is deleted due to failure,

180 the explicit dynamic equilibrium equation is used for the analysis, which is based on Central

181 difference method of Bathe (1996) as follows:

182
$$M\ddot{u}_t = P_t - (I_t + I_{td}) \quad (11)$$

183 Where

184 \ddot{u} is Nodal acceleration matrix,

185 M is diagonal matrix of mass,

186 P_t is matrix of external force at time t,

187 I_t is matrix of internal force at time t,

188 I_{td} is matrix of force loss due to structural elements failure

189 Therefore, the acceleration can be worked out as

190
$$\ddot{u}_t = M^{-1} [P_t - (I_t + I_{td})] \quad (12)$$

191 Hence, the velocity can be calculated by interpretation of the acceleration using central difference

192 method:

193
$$\dot{u}_{t+\frac{\Delta t}{2}} = \dot{u}_{t-\frac{\Delta t}{2}} + \frac{\Delta t_{t+\Delta t} + \Delta t_t}{2} \ddot{u}_t \quad (13)$$

194 Similarly, the displacement of all the nodes at certain time can be calculated through the
195 interpretation of the velocity.

196 When displacement of the fibre is determined, the strain increment of the fiber can be worked out
197 using the displacement divided by the cross-section area of the fiber. The strain increment and
198 initial strain will be substituted into formula (4) or (6), therefore, new stress and damage value in
199 each fiber can be obtained by iterations.

200

201 The method of the authors (2010) is used here to simulate the buckling and post-buckling behavior.

202 In the model, each beam element is divided into 4 segments along its length, and all the segments
203 are arranged along a half-wave sine curve to simulate the initial imperfection.

204 This method is very effective in simulating the buckling and post-bulking behavior. The buckling
205 load from the modelling result is less than 5% difference to that of the Chinese code (2003), which
206 satisfies the requirement for earthquake analysis. Above theory is also incorporated into the
207 subroutine VUMAT program in ABAQUS.

208 ***Validation of the numerical method***

209 In order to validate the proposed numerical method, a full scale hysteretic test which is conducted
210 by the first author of this paper in collaboration with Prof Li Haiwang from Taiyuan institute of
211 technology is used here. As shown in Figure3, an arch truss with span of 5800mm, height of 1200m
212 and depth of 300mm was tested, Chinese Tubular Section $\text{Ø}88.5 \times 3.75$ and $\text{Ø}75.5 \times 3.5$ were used for
213 top and bottom cords, $\text{Ø}60 \times 3.25$ were used for diagonal members. The grade of the steel is Chinese

214 Q235-B. The Arch truss was supported at the two ends with load applied at the center, as it shown
215 in Figure 4. Tensile tests were also conducted from coupons taking from the arch truss, the material
216 parameters are shown in Table 1. The time history of the applied load is shown in Figure 5. When
217 applying the load, the load control method is used in the first 9 cycles, followed by displacement
218 control in the remaining cycles.

219 The above tests were simulated using the numerical modelling techniques developed in this
220 research. As it shown in Figure 6, a model replicates the full-scale test has been setup. In the
221 simulation, the same sections for the structural members and same steel grade were selected. In
222 addition, the same loading regime of the experimental tests was applied. The load was applied at the
223 same position of the test, as it is shown in Figure 7, which also shows the numbering of each fiber.

224
225 The comparison of the result from the numerical modelling and full-scale test is shown in Figure 8,
226 which shows the comparison of hysteretic curve between the test and the numerical modelling result.
227 It can be seen that, good agreement is achieved. It can also be seen from Figure 8a that the stiffness
228 of the structure when the vertical displacement reached 16mm is smaller than that the stage that the
229 displacement is 13mm. , This is due to the stiffness degradation resulted by Damage Accumulation.
230 Therefore, the damage accumulation should be considered in the numerical simulation for obtaining
231 more accurate results. The modelling result of Figure 8b also shows the similar stiffness degradation,
232 this
233 proved the capacity of the proposed model to accurately capture the stiffness degradation due to the
234 damage accumulation.

235

236 During the test, when the vertical loading displacement increase to 35mm, cracks were observed at
237 the top chords which locate near the support as it shown in Figure 9a. With the increasing of the
238 loading, the crack was further developing (Figure 9b), in the meantime, crack was also observed at
239 the joints of the diagonal members, as it is shown in Figure 9 c. When the loading displacement
240 increased to 47mm, rupture of the top chord occurred as it shown in Figure 9d. The numerical
241 simulation also captured the similar cracking pattern.

242

243 The results of top chord member 296 and diagonal member 288 are shown in Figure 10, which are
244 extracted from the model. As it is shown in Figure 10a, at time 334 s, when the displacement is 30
245 mm, the maximum value of the damage D is observed in chord member 296 and $D > D_{\text{limt}}$, which
246 indicates the fracture of member 296. Similarly, the fracture of member 288 is also observed at time
247 340s when $D > D_{\text{limt}}$ is observed, as it is shown in Figure 10. the correspondent displacement was
248 found to be 35mm in the modelling result as it is shown in Figure 11, and these two fractured
249 members were deleted in the model by the program during the simulation.

250

251 From above comparison, it can be seen that, the proposed model can accurately simulate the
252 response of the full-scale test.

253

254 **Progressive collapse analysis under earthquake loading**

255 In order to investigate the collapse mechanism of the reticulated dome, as it is shown in Figure 13, a
256 40m span single layer Kiewitt shell with 6 rings, 8 meters high, is modelled. Kiewitt shell is one of
257 the typical grid configurations for lattice shell. As discussed in Melaragno (1991), Kiewitt shell

258 contains the advantages of other type of shell such as Schwedler lattice shell and union type shell.
259 Kiewitt shell has uniform grid, which contains relatively good mechanical properties such as higher
260 bearing capacity for the seismic load. The live load of the roof is taken as 2.5KN/m^2 . The dome is
261 pin supported along the circumference. All the structural members are Chinese Steel Tubular
262 Sections, the members in the radials are Chinese $\text{Ø } 165 \times 5$, and the remaining sections are Chinese
263 $\text{Ø } 140 \times 4$. The material properties are listed in Table 2.

264

265 In the simulation, all the structural members are modelled using beam elements. Each beam element
266 is divided into 4 segments along its length to model the buckling behaviour. In addition, each beam
267 element is sub-divided into 8 fibres across its cross-section.

268

269 The analysis is divided into two steps. The first step is static analysis, where the gravity load is
270 applied to the structure. The second step is dynamic analysis, where the time history of Northridge
271 earthquake (as it is shown in Figure 12) was applied at the support, in X, Y and Z direction, with the
272 Peak Ground Acceleration (PGA) of 1600gal in X direction, 0.85 times 1600gal in Y direction and
273 0.65 times 1600gal in Z direction, respectively. The time duration is 15s, which is greater than 10
274 times the natural period of the structure.

275

276 ***Modelling results***

277 Figure 13 shows the process of the collapse of the dome. It can be seen that, at 9.25s, all structural
278 members are still in the elastic stage. At 9.75s, the GPA reaching the peak value, local structural
279 members failure was observed at area, the local failure propagated further until 11s, when half of

280 the dome collapsed. Figure 14 shows the sequence of the structural member failure before 11s. It
281 can be seen that, the member failure started at the outer rings of the domes and then propagated to
282 the center of the dome.

283

284 Figure 15 is the time history of the vertical displacement of node 1 and node 591 (their location are
285 shown in Figure 13), where node 1 locates at the centre of apex, it can be seen that, at 12 s, the
286 vertical displacement of node 1 increased dramatically, which indicted the collapse of the whole
287 dome. However, node 591 experienced a two-stage collapse as it shown in Figure 15.

288

289 Figure 16 shows the response of the axial force of structural member 219 and 787 (their locations
290 can be found in Figure 14), the two time histories are coincide at the beginning, however, element
291 219 drop to zero at 10.05s, element 787 is kept intact.

292

293 As it is introduced in the earlier section, the judgement of failure of the structural element is based
294 on the value of damage accumulation of all the fibres. Figure 17 shows the stress development of
295 the fibre number 0 and number 90 in element 219 and 787. From Figure 17a it can be seen that, the
296 effective stress of fibre number 0 in element 219 entered yielding level after 3.37s. At 9.725s it
297 failed, the effective stress dropped to 0. Similarly, in Figure 17b, it can be seen that, fibre number 90
298 failed at 10.05s. It can be concluded that, the damage accumulation is correlated to the numbers of
299 the cyclical loading and the magnitude of the loading. From Figure 17c, it can be seen that, no
300 failure is overserved in Element 787.

301

302 Figure 18 shows the damage value D for each fiber in element 219 and 787. It can be seen that, the

303 value D of these fibers in element 219 all reached 0.209 before 10.05s, however, from Figure 17a
304 and b, it can be seen that, the effective stress dropped to 0 at the final stage, which indicate the
305 failure of the fiber. However, the maximum D value of the fibers in element 787 is only 0.104
306 therefore, failure is not developed.

307

308 ***Discussion on Collapse mechanism***

309 Figure 13 depicts deformation and damage distribution during collapse process, where the
310 distribution of the D value can be checked. It can be seen that, under the earthquake, the collapse
311 process of the dome can be divided into three stages:

- 312 1. The first stage, most structural members in the dome remain as elastic, some members
313 developed into plastic stage(0-9.5s)
- 314 2. With the accumulation of the damage developed, fracture in some structural members were
315 observed, the stiffness of the whole structure reduced, excessive displacement was
316 developed in local area and therefore, the subsidence of some structural members is
317 observed in the local area.
- 318 3. The collapse is then propagated to a larger area during the time of 9.75-11s. The collapse
319 of the whole structure started after 11s.

320 It can be seen that, the damage development in the structural member during these three stages are
321 different, their deformation also varies, however, there is no sharp division can be found between
322 these three phases.

323 ***Parametric study to investigate the collapse mechanism***

324 In order to further study the collapse mechanism of this type of structure under earthquake

325 loading, based on the proposed model, a parametric study is made with parameters of different
326 span, span to depth ratio, live load, as it shown in Table 3. Two different types of shells K6 and
327 K8 were investigated under different time history of earthquake loading and different loading input
328 directions, as it shown in Table 3. Three time histories: Taft、 El-central、 Qianan (China) were
329 chosen in the simulation. The earthquake motions were input in 0° , 30° , 45° , 90° directions.

330

331 As it shown in Figure 19, only the modelling results of dome K8 (with span/ depth of7/1) and K6
332 (with span/depth 7/1) are shown here. Both have the similar collapse mechanism as it is discussed
333 in the earlier section

334 The results from above parametric studies show that, very similar collapse mechanism as it shown in
335 Figure 13 were observed. This indicates that, the collapse mechanism is not sensitive to model
336 parameters. All the models exhibit the similar three-stages collapse pattern as it is shown in Figure
337 13.

338 **Conclusion**

339 Based on the results and analysis in this paper, the following conclusions can be drawn:

- 340 1. A new modelling technique based on fibre beam element method is developed to model
341 the behaviour of individual structural members of reticulated shell.
- 342 2. The failure criteria of structural members based on damage accumulation theory is
343 developed and is validated based on the full-scale tests, it shows that the proposed model
344 can accurately simulating the stiffness degradation due to damage accumulation and
345 failure modes of each structural member.
- 346 3. The numerical method is developed based on the VUMAT to model the global response

347 of a truss under cyclic loading and validated against test result, good agreement is
348 achieved.

349 4. The progressive collapse analysis of single layer reticulated dome under severe
350 earthquake is performed and the response and the collapse mechanism of single-layer
351 reticulated shells under the severe earthquake are discovered.

352 5. A three-stages collapse mechanism were discovered. It is also found that this three-stages
353 collapse mechanism is consistence for different model parameters such as: different
354 types of the domes, different span/depth ratios, different earthquake time histories.

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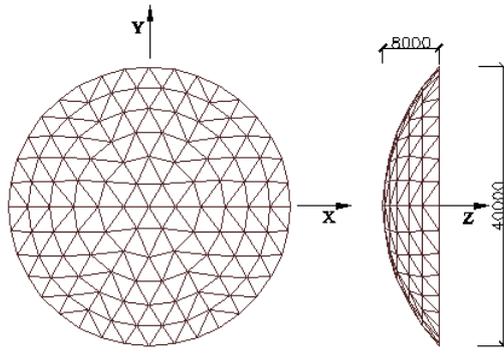


Figure 1 The prototype model

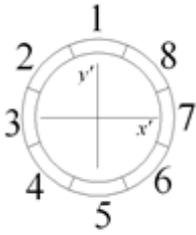


Figure 2 Subdivision of beam element into fibers

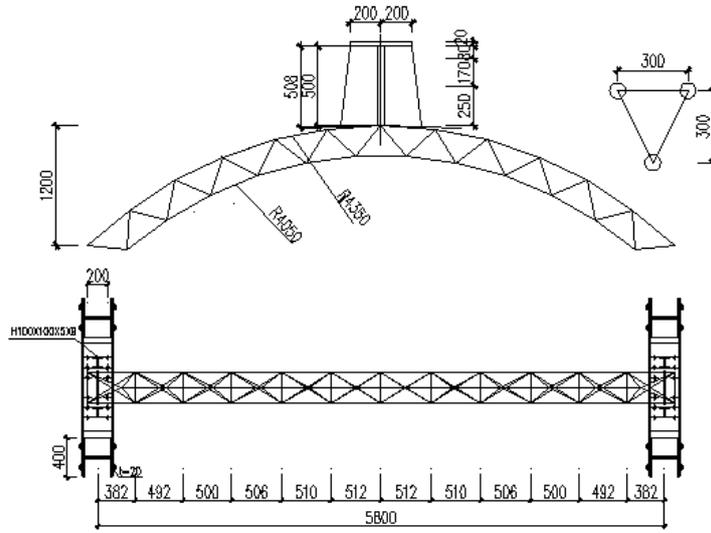


Figure 3 Design drawing of Arch-truss model



Figure 4 Hysteresis loading test on arch-truss

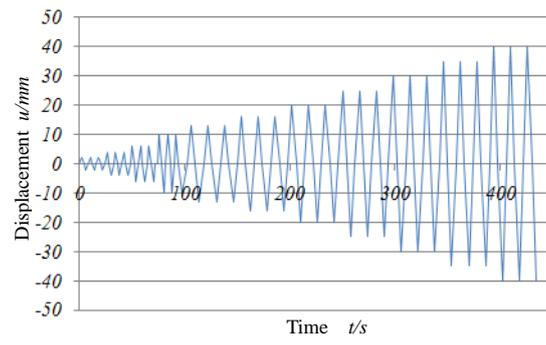
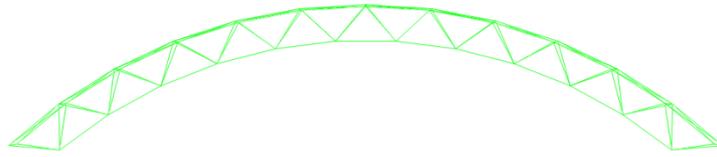
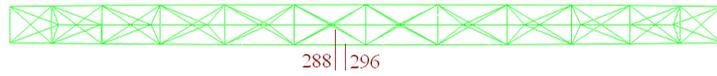


Figure 5 Time history of loading



a Main view



b Top view

Figure 6 Validation Model

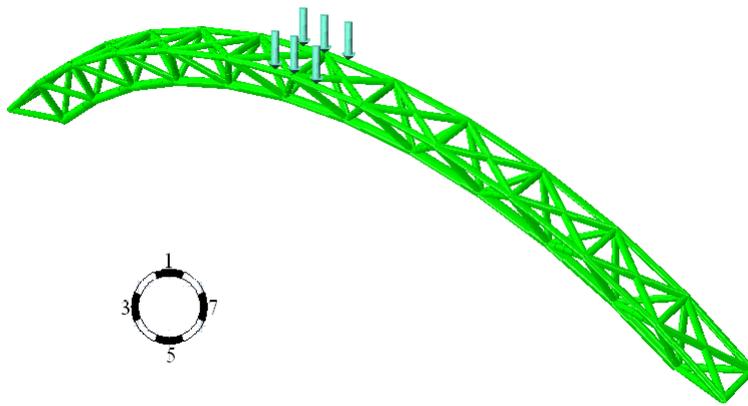
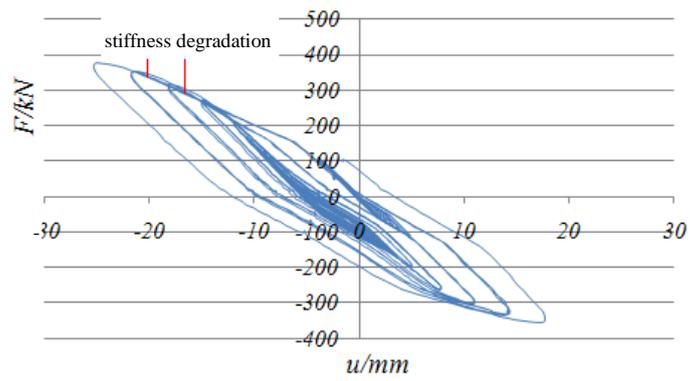
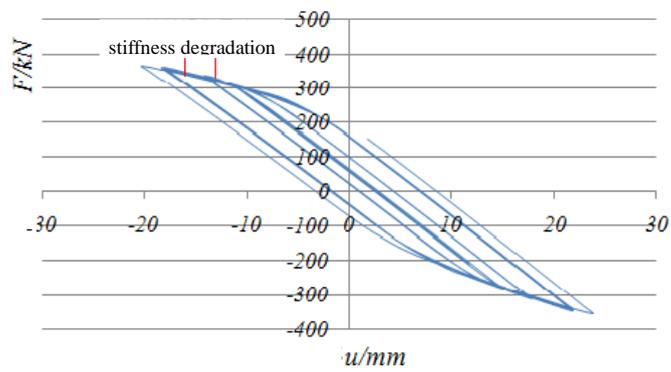


Figure 7 Numerical Model



a Hysteric-curve from test



b Hysteric-curve from numerical model

Figure 8 Comparison between the test result and modelling result



a Initial Crack development at support location



b Further development of the crack at support location

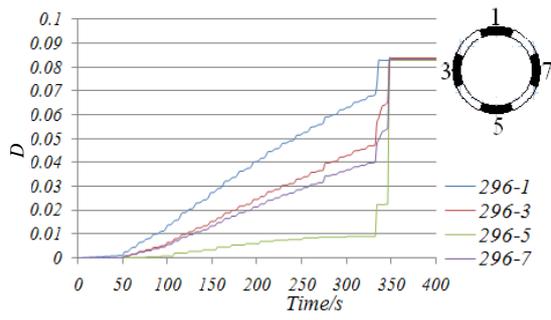


c Crack on the joints of diagonal member

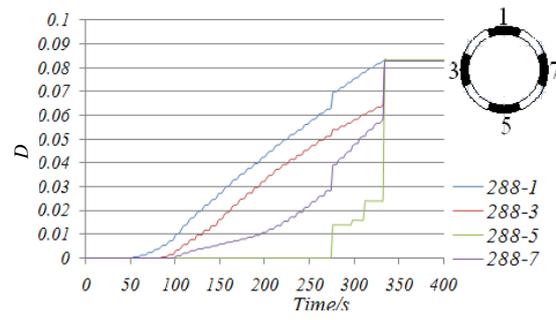


d Fracture at middle of top chord

Figure 9 Fracture process of arch-truss



a member 296



b member 288

Figure 10 Fiber damage - time history curve (showing the result of fiber1, 3, 5, 7 for each element)

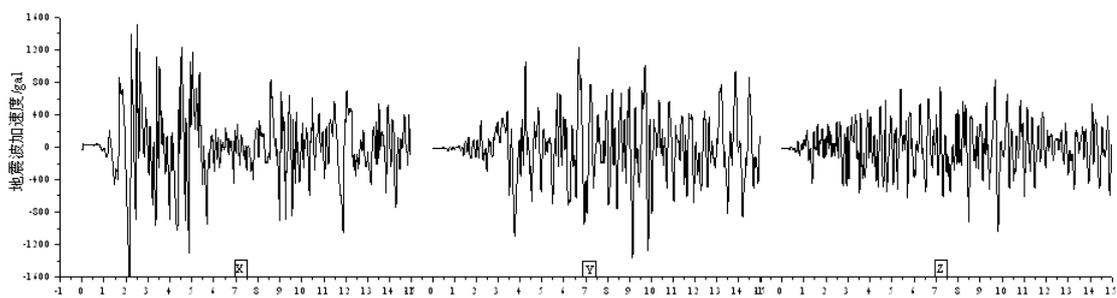


Figure 12 Ground Acceleration-Time history in X, Y and Z direction

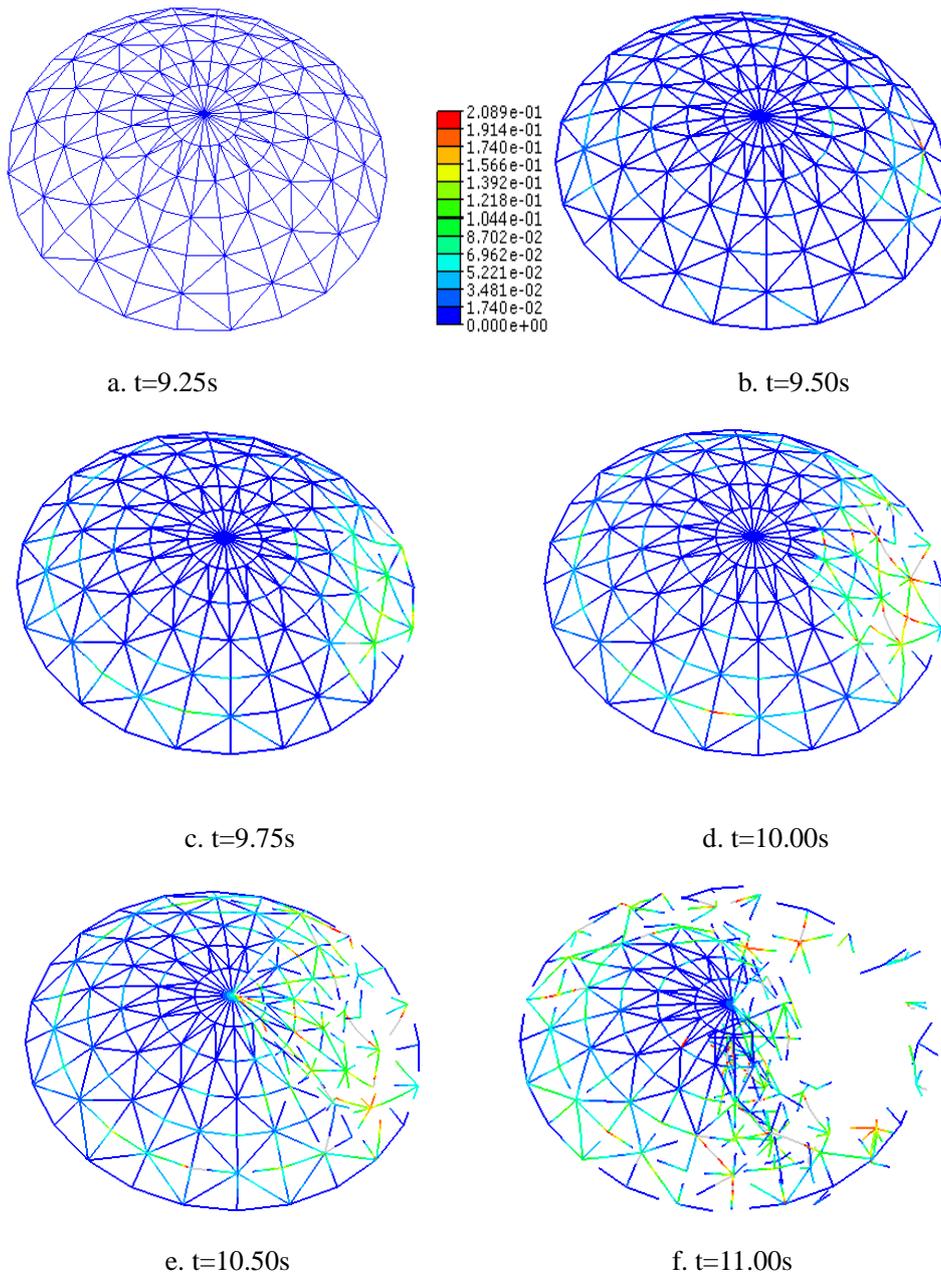


Figure 13 Deformation and damage distribution during collapse process

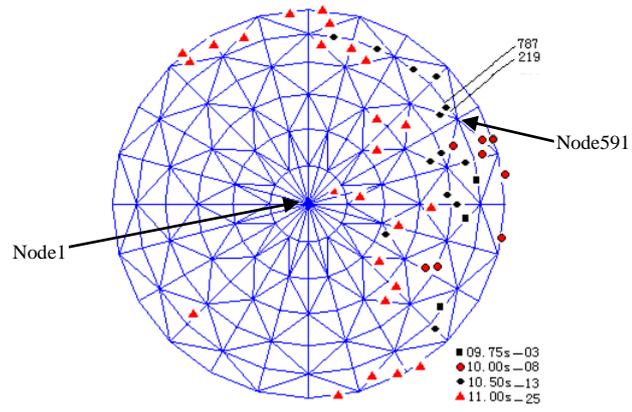


Figure 14 Element failure process

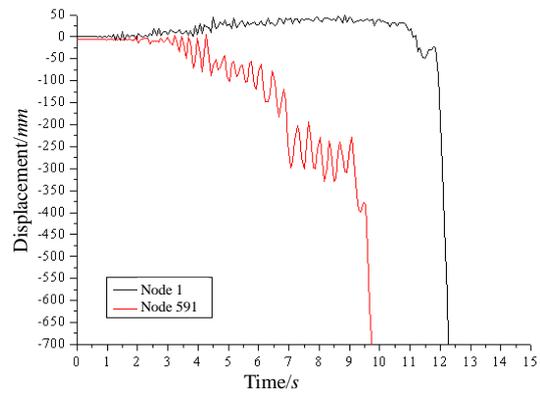


Figure 15 Node displacement-time history curve

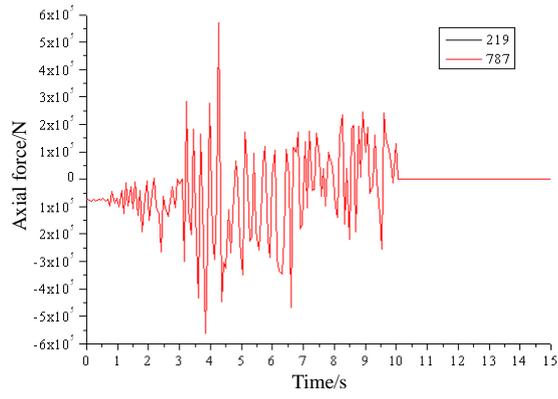
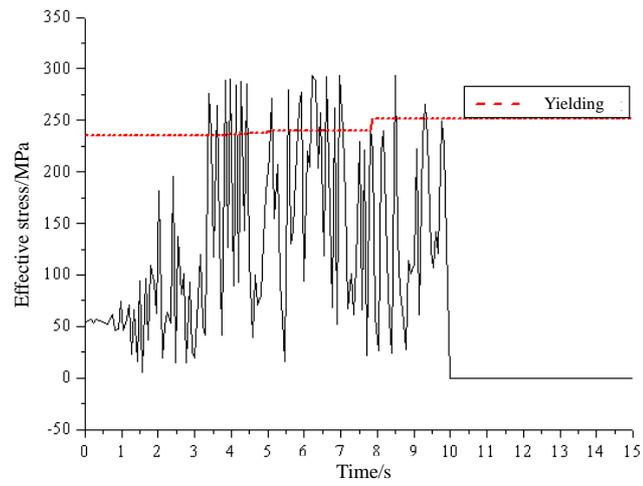
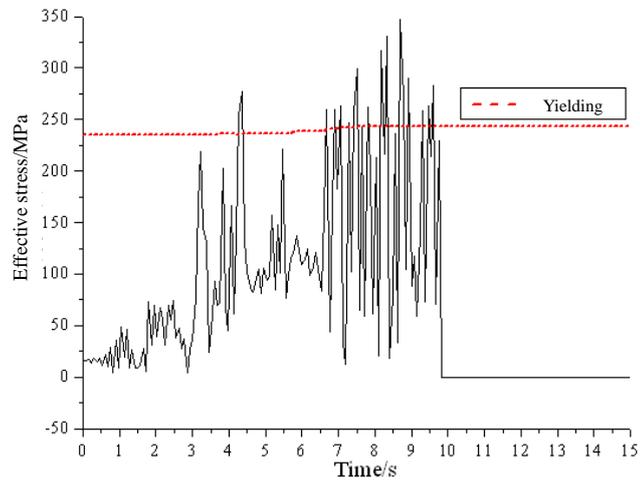


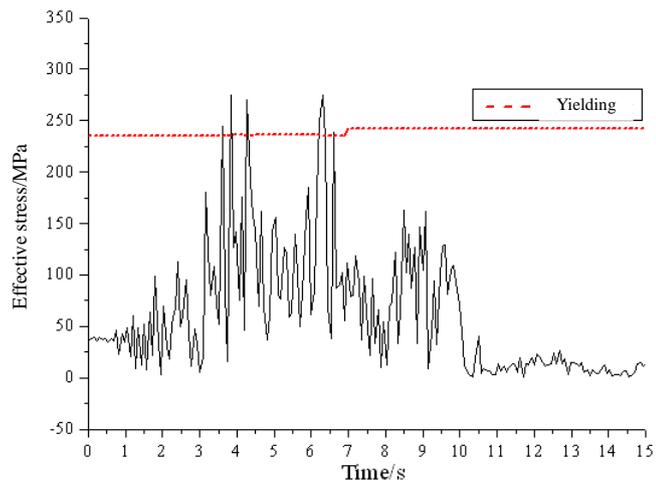
Figure 16 Time history of response of axial force in element 219 and 787



a fiber 0# in element 219



b fiber 90# in element 219



c fiber 0# in element 787

Figure 17 Time history curve of Effective stress in element fiber

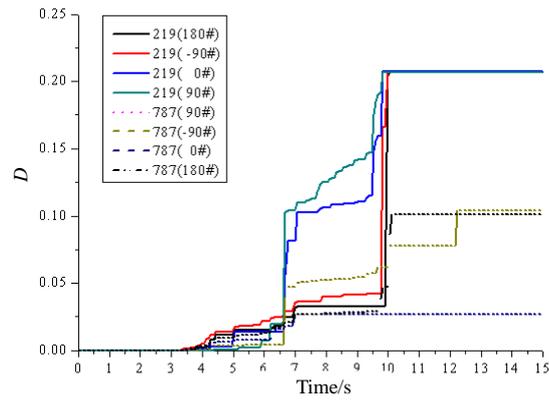
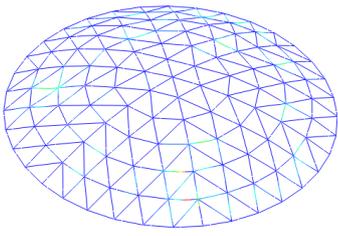
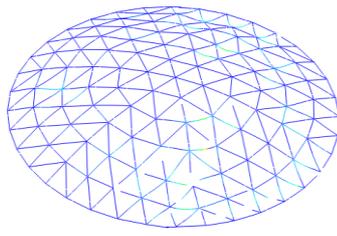


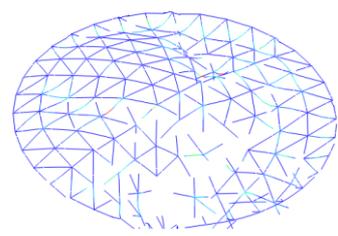
Figure 18 Time history of fiber damage



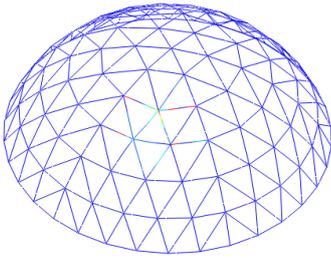
a1 K8 Subsidence appear



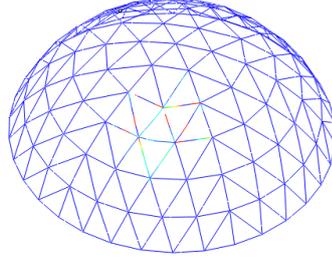
a2 K8 Subsidence develop vertically



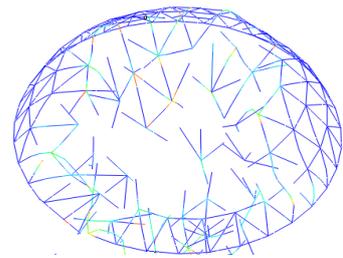
a3 K8 Subsidence develop quickly



b1 K6 Subsidence appear



b2 K6 Subsidence develop vertically



b3 K6 Subsidence develop quickly

Figure 19 Deformation and damage distribution during collapse of Kiewitt shells(a span /depth ratio 7:1, b span/ depth ratio3:1)