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Analysis of Fiber optic sensor embedding in metals by automatic and manual TIG welding

T. Grandal, A. Zornoza, A. López, S. Fraga, T. Sun and K. T. V. Grattan

Abstract— In this paper, the embedding of fiber optic sensors in metals, by using both automatic and manual Tungsten Inert Gas welding (TIG) is discussed for nickel- and copper-coated Fiber Bragg Gratings (FBG) written into an optical fiber, as embedding such sensors in metals provides protection against environmental effects. In the investigation and analysis of the performance of a number of such sensors, copper-coated sensors were seen to lose their temperature and strain sensitivity while being embedded due to damage to the coating, while with a nickel coating the sensors in the fiber were found to withstand the process with a lesser effect on the sensor performance. The research has also shown that the Automatic TIG process used is less invasive than the manual TIG approach, although more expensive to implement.

Index Terms— Fiber optic sensors, metal embedded fiber optic sensors, TIG welding, Fiber Bragg Gratings.

I. INTRODUCTION

The fourth industrial revolution, also called Industry 4.0, requires sensor integration in tools, materials and machines for accurate, real time monitoring of many important systems and processes. Prior research has found that with composite materials, sensors can be easily embedded during the manufacturing process and they have, for example, been used successfully by some of the authors for the monitoring of innovative composite bridge structures [1]. In many cases, cheaper conventional sensors such as piezoelectric accelerometers, strain gages or thermocouples can be employed if the monitoring conditions suit, although there are a number of specialist areas where this is not the case and optical fiber methods are to be preferred [2,3]. For metals, however, it can be a real challenge to incorporate sensors effectively: the manufacturing process operates at high temperatures and applications often include harsh environments, which conventional sensors are not easily able to withstand. Fiber optic sensors (FOS) present numerous advantages that suit them well to operation in these harsh environments, where issues

such as electromagnetic immunity, small size, the possibility of multiplexing many sensors and simultaneous monitoring several parameters in different positions in one single fiber are critically important [2].

In most current applications, usually FOS are glued on the surface of metals, as typically is done in the monitoring of bridges and reinforcement bars [3] but the long-term degradation of adhesives and glues can affect the measurand, often then inducing unexpected errors, for example those caused by a decrease in the strain transfer as the adhesion weakens. Embedding FOS into metallic structures can avoid these problems (and the consequent resultant errors) and thus the challenge of creating a satisfactory and reproducible way to do this must be tackled. The experience of the authors has shown that to be effective when embedding an FOS into metallic materials, the fiber must be coated with a metal layer. Such a coating mechanically protects the fiber from the high temperatures and mechanical loads experienced during the embedding process [4]. In addition, they affect the bonding to the metal, which can be compromised by slippage or delamination [5], [6]. The earliest solutions presented for embedding FOS into metals were based on deposition techniques. In this case, the total diameter of the fiber needed to withstand the embedding process was often as large as 2mm, making it significantly larger when compared to typical communications-based optical fiber (cladding $\sim 125\mu\text{m}$ diameter) [7]. Ultrasonic welding and vacuum brazing have also been proved to be valid solutions for joining the fiber to metal, although the low temperature of the process limits the application of the sensors in the first instance [8] and the complexity, cost and need for a vacuum chamber limits the flexibility of the second [9]. Techniques based on Selective Laser Melting have shown promising results due to the possibility there is for precise thermal control of the process, to create protective coatings of up to $350\mu\text{m}$ total diameter [5], but it is hard to expand this to production levels and be sufficiently flexible for different materials to be used. Finally, an

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embedding process using a laser beam to create a cladding has also been demonstrated to provide flexibility in manufacturing, since no vacuum or gas chamber is needed for the process and optical fibers with nickel coatings (of total diameter $\sim 300\mu\text{m}$) can be successfully embedded [10]. However, the employment of high-power lasers for this LMD (Laser Metal Deposition) process, to create the necessary level of heating needed, makes the technique very expensive.

It is clear that more cost-effective and simpler techniques, better suited to use eventually in a production environment are required. In this paper the use of Tungsten Inert Gas (TIG) welding is discussed as an effective means to achieve FOS embedding in metals, at low cost and in a way that makes it suitable for using in a number of different applications. TIG welding is an arc electric welding process, involving the use of a shielding gas and a non-consumable tungsten electrode [11]. The arc is established between electrode and the piece to be welded, and filler metal can be added independently. Two different TIG welding variants are studied in this work to evaluate which is the most effective, these being both automatic and manual welding. In the automatic TIG welding process, the parameters involved in the process are selected prior to the use of the welding process. By contrast, in the TIG manual process, it is only the current used which is *a priori* defined, with all the other parameters for the welding conditions usually depending of the experience of the technician undertaking the weld, based on the techniques familiar from the literature [11]. Repeatable and high accuracy automatic TIG welding techniques are available, as is the less repeatable, yet highly-adaptable and portable manual TIG welding technique. Both techniques are low-cost in comparison to the other techniques used for FOS embedding and have the advantage of being familiar, being used in many industries in the metal-mechanic sectors, this being especially true of the widely-used manual TIG approach.

In this work, to evaluate and optimize the techniques described to create metal-clad sensors, Fiber Bragg Grating-based sensors (FBG) in optical fiber have been chosen, as these are widely used in many different sensor applications [12] where ruggedized sensors are needed. FBGs can easily be designed and written into a short, 5mm length of optical fiber, forming the basis of the sensor. As high temperatures are reached during the welding processes studied, the FBG-based sensors selected where written by using a femtosecond laser to ensure they survived that heating process. Thus FBGs were designed to withstand temperatures up to 1000°C , without the danger of the grating being erased or damaged by the welding process. The design of embedded sensors discussed will allow them to operate by reflecting light on a narrow wavelength band (less than 1pm) from the incident white light signal, monitoring the reflected wavelength variation caused by changes such as in temperature and strain. FBG-based sensors have been used for different applications, over many years, where metal embedding of FOS

has been shown to be particularly valuable [3], [5]-[9] and thus are an ideal choice for the sensors demonstrated in this work.

II. EXPERIMENTAL SETUP

As has been discussed in the Introduction, TIG welding is an arc electric welding process using a shielding gas and a non-consumable tungsten electrode, where an electric arc is established between the electrode and the piece to be welded, allowing filler metal to be independently added. For this work, the added material used comes from a wire of 1.6mm diameter tin alloy, with composition $\text{Sn}7.5\text{Sb}3.5\text{Cu}$. This alloy has a melting point of 250°C , but during the welding process higher temperatures are achieved, up to 700°C . The specimens into which the optical fibers and sensors are embedded are made of forged steel, type ST52, with a thin alloy coat as the metal, into which coating the FOS are embedded.

The materials chosen for the protective coatings for the sensors were nickel and copper (due to their high melting points, durability, cost and ease of use). In addition, these metals have already been used in previous studies and a good performance has been achieved with them [10], [11]. While evaluating the many techniques reported to coat optical fibers [4]-[6], it was found that the same techniques reported by us previously in the literature [10] were the most suitable and thus were chosen. In this process, first a layer of gold of $2\mu\text{m}$ thickness was deposited on the optical fiber using a sputtering process. This layer gives the optical fiber the necessary conductivity prior to the application of the second step, where it is coated with nickel or copper, achieving the desired thickness by use of electroplating deposition. The embedding strategy for the sensor-based fibers produced using each of the techniques is explained in detail below.

A. Automatic TIG Embedding process

In Fig. 1, the automatic TIG welding setup which was employed in this work is shown. An automatic TIG welding set-up with an FMW-Multi Welding System (Fronius), Magic Wave 5000 and KD 1500 D-11 and a torch, also from Fronius, were used as the welding machine and the device to guide the wire, respectively. During the embedding trials, the optimum welding conditions established from our previous experience

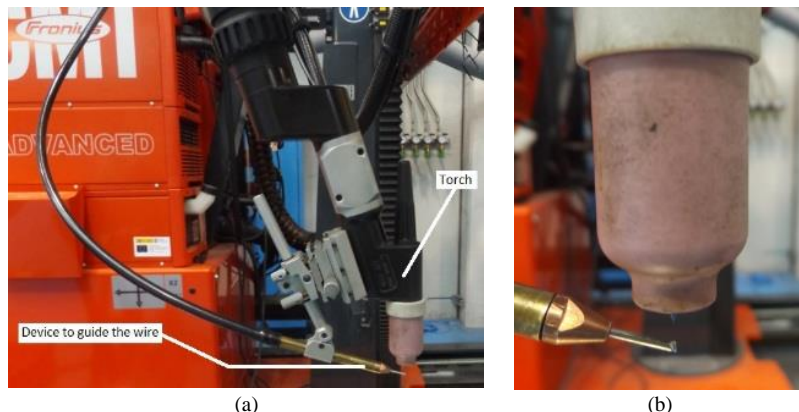


Fig. 1. (a) Automatic TIG welding setup used in this work showing the device to guide the wire and the torch and (b) a close-up of this key part of the set up.

were set, these being: a wire diameter of the tin alloy of 1.6mm; the use of a non-consumable electrode of 1% lanthanum (class EWLa-1 according to the American Welding Association) with 1.6mm diameter; as shielding gas 100% Argon; a direct pulsed current and with the electrode connected to the negative pole. The other main TIG operational parameters which were adjusted to achieve this optimum embedding process were as follows: an average current of 35-40A; a travel speed of 0.4 m/min; a wire speed 1.5 m/min and a torch position relative to the fiber of 1.5-2mm.

B. Manual TIG embedding process

In Fig. 2, the manual TIG welding setup employed in this work is shown. This had been used in some of our prior work [11], in which the optical fiber containing the sensors was positioned on top of the material on which it is to be embedded and the wire from the TIG was melted on top of, or close to, the optical fiber. Our previous experience has shown that manual TIG embedding of optical fibers and sensors should be performed by a skilled technician as, being a technique with a significant component of operator skill, experience and know-

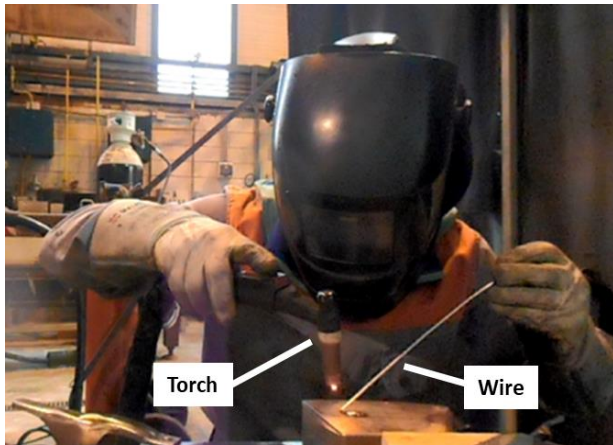


Fig. 2. Illustration of the manual TIG welding set-up

how, the technician's skill brings these key elements for the success of the process and thus in regularly achieving a 'good weld'.

III. RESULTS

A. Embedding optical fibers

One of the main advantages of the use of FOS is how minimally invasive they are, due to their small size. For example, with TIG embedding, once the optical fiber or sensor is embedded, the total thickness of the tin alloy-coated layer in the forged steel specimens is still very small, at ~3mm. However, the metallic coating needed for protection in the metallic embedding process compromises this, so one parameter of interest is the minimum embeddable coated optical fiber diameter that ensures that both the integrity of the fiber and sensor are maintained, while the fiber is kept minimally invasive. Thus, its presence does not compromise the usability of the manufactured metallic part. In the case of using automatic TIG, several tests were performed (based on the process described in our prior work [10]) to estimate the

minimum coating needed for successfully embedding the optical fibers and sensors. A first step was to use relatively coarse tuning, with different coating thicknesses on the optical fibers to help to define the best embedding strategy. In this first step a 'red-light' optical fiber fault detector was used to estimate any damage caused to the optical fiber by the process. In the second step, various optical fibers with different thicknesses were embedded and any loss of the fiber was monitored, this being an indicator of the damage suffered by the optical fiber itself. For the manual TIG process, the results reported in prior works were supplemented with those created from new tests [9]. Thus, the minimum embeddable diameters, determined as a function of the technique used and the coating material employed, are listed in Table I. It should be noted that nickel coatings of lower thicknesses than before can be embedded, this being attributed to the higher melting point (1455°C) for nickel, when compared to that for copper (1085°C) and to the thermal conductivity of each material. The thermal conductivity of the Cu is higher than that of Ni, which makes that the heat generated during the welding process travel faster to the fiber cladding and core, causing damage to the fiber if the coating layer is not sufficiently thick. Also, the Automatic TIG process allows lower coating thicknesses to be used than for the manual TIG, this being attributed to the greater accuracy achievable from the automatic TIG process and because is a faster process (where the high temperatures reached can dissipating faster avoiding the fiber damage).

TABLE I
MINIMUM COATING DIAMETERS OF SUCCESSFULLY EMBEDDED OPTICAL FIBERS

Coating material	Minimum embeddable coating diameter of optical fibers (μm) $\pm 5\mu\text{m}$	
	Automatic TIG	Manual TIG
Nickel	236	322
Copper	279	426

B. Embedding FBGs

To evaluate the performance of the embedded optical fiber sensors created, metal-coated FBGs were embedded in metallic specimens, these being designed to allow temperature and tensile tests on them to be performed. The FBGs used in the work were manufactured by using a femtosecond laser-based manufacturing process (from Femto Fiber Tec), where the grating was of 5mm length and the optical fiber for this sensor was type SMF-28. The FBG fabrication process used was chosen (over the use of a nanosecond phase mask-based method) to allow them better to withstand the high temperatures of the embedding process [1] with the coating process described in Section 2. The FBG coatings were chosen to have sufficient thickness to withstand the embedding process, this being based on our previous experience, as described in Section 2. Four FBGs were used these being as follows: (a) a 464 μm total diameter nickel-coated FBG with automatic TIG embedding; (b) a 592 μm total diameter copper-coated FBG with automatic TIG embedding; (c) a 526 μm total diameter nickel-coated FBG for manual embedding and (d) a 738 μm copper-coated FBG, again for manual TIG welding. With such FBGs, the

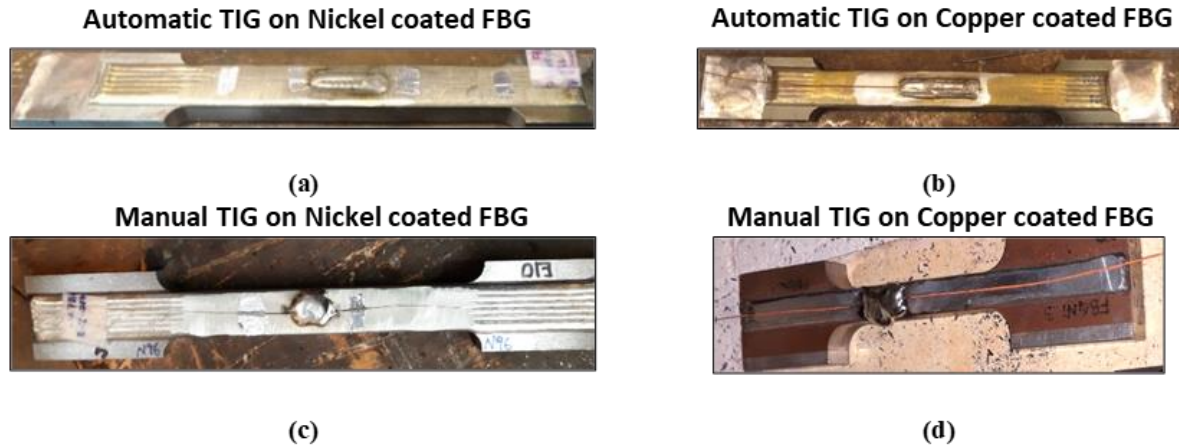


Fig. 3. Samples with embedded FBGs created as described above by (a) automatic TIG on nickel-coated FBG, (b) automatic TIG on copper-coated FBG, (c) manual TIG on nickel-coated FBG and (d) manual TIG on copper-coated FBG.

performance of metal embedded sensors obtained with both the automatic and manual TIG and both copper- and nickel- coated FBGs can readily be compared. In Fig. 3, the four specimens with the embedded sensors using TIG welding are shown, where the better accuracy achieved in the deposition of the metal can be observed for the automatic TIG embedded FBGs, (Fig. 3(a) and (b)), than is seen for the manual TIG embedded specimens, (Fig. 3(c) and (d)). The embedding depth for each FBG sensor is a little different, as Table II shows, despite the fact that the diameter of wire used as the added material was the same for all of them.

FBG-based sensors are widely used for their sensitivity to strain and temperature. Recognizing this, three characterization tests were performed on the embedded sensors, as follows: (1) a spectral analysis of these embedded sensors before and after having been embedded, (2) temperature tests in a Lentong TLK38 oven; (3) tensile tests in an MTS landmark 250kN tensile testing machine and (4) destructive metallography tests. The first of these tests, (1), (2) and (3), have been used to help evaluate the performance of the embedded FBGs and the last, (4), the quality of the embedding process itself.

1) Spectral analysis

A first method used to evaluate the quality of the process of embedding of the FBG sensors is to analyze and compare the spectrum of the sensors before and after having been embedded. In the Fig. 4, the spectra for the coated FBG sensors before and after being embedded are shown. It can be noted that here the femtosecond laser-written FBG sensors have a spectrum that is wider (at 0.75nm, FWHM) and of lower reflectivity than the UV-laser written FBG sensors. Further, as Fig. 4(b) shows, the signal amplitude observed after the metallic coating is applied is lower than that in the previous case and the sensor is compressed because of the coating layer. In the case of the sensors embedded by using the automatic TIG welding process (Fig. 4(a) and 4(b)), the wavelength variation seen is around 2nm after the embedding process occurs. In this case, the signal amplitude has fallen, while the peak shape is similar to that seen previously. Looking these spectra, it would appear that the FBG sensors are well embedded, with a good bond from the

added and the base material. However, in the case of the FBG sensors embedded by using the manual TIG welding process, the sensors are more affected. Here, the spectra observed after the embedding process has occurred show a lower amplitude and in the case of the Cu-coated FBG sensor, the peak presents a high level of asymmetry. The wavelength shift for the Ni coated FBG sensor embedded by manual TIG welding (Fig. 4(c)), is around 2nm, similar to the previous sensors embedded by use of the automatic TIG welding process. However, for the Cu-coated FBG sensor, the wavelength shift is around 8.5nm, which is a higher variation, in comparison to what previously was observed. From these results, is easy to conclude that the Cu-coated FBG sensor, embedded by using manual TIG welding has a poor adhesion with the base and the added

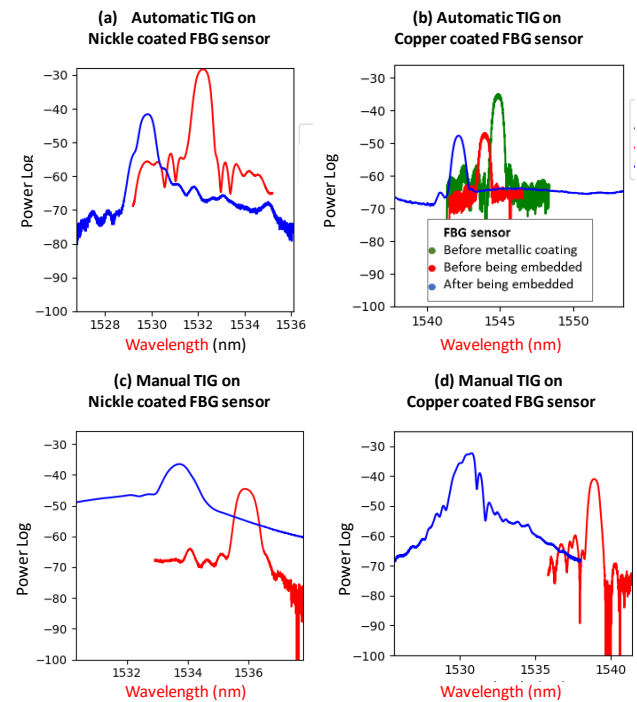


Fig. 4. Spectra taken after and before embedding process for (a) automatic TIG on nickel-coated FBG, (b) automatic TIG on copper-coated FBG, (c) manual TIG on nickel-coated FBG and (d) manual TIG on copper-coated FBG.

material or the coating layer has deteriorated during the embedding process. Additionally, it is possible to determine that the manual TIG process is more aggressive when used with the metallic coated FBG sensors, than does the automatic welding process.

2) Temperature tests

To evaluate their temperature performance, the specimens created with the embedded sensors were evaluated over the range from 50°C to 200°C, in steps of 30°C. This ‘thermal steps’ test was repeated three times to ensure the repeatability of the performance of the embedded sensors. The maximum temperature of the tests was limited by the tin alloy melting point, to that temperature of 250°C. The results from the calibration steps are shown in Fig. 5 (a) to (d). A linear fit was observed for each sensor and ‘thermal step’ in order to obtain the thermal sensitivity for each. The response with wavelength is depicted in Fig. 6(a) to (d), for each specimen. The sensitivities measured are repeatable over the three calibration tests undertaken and the results are summarized in Table II.

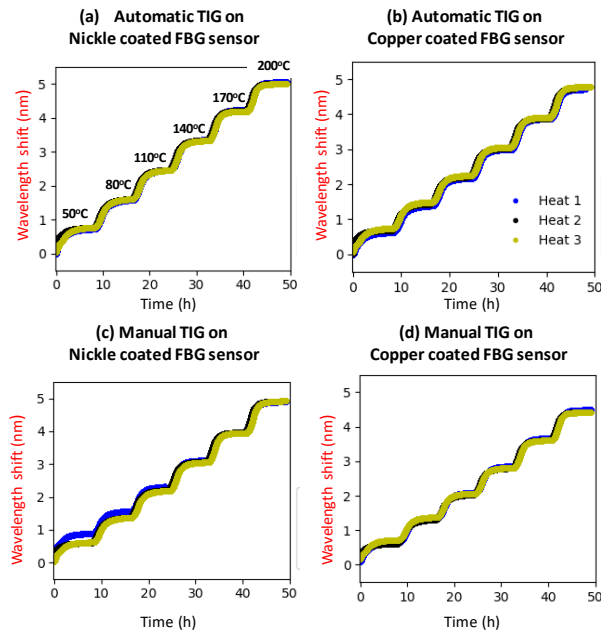


Fig. 5. Temperature tests on the embedded FBGs for (a) automatic TIG on nickel-coated FBG, (b) automatic TIG on copper-coated FBG, (c) manual TIG on nickel-coated FBG and (d) manual TIG on copper-coated FBG.

Additionally, to obtain the thermal sensitivity *before the coated FBG sensors were embedded*, the same thermal test step, as used above was performed. As Table II shows, only for the Ni coated FBG sensor embedded by using the Manual TIG, was the same thermal sensitivity obtained as was seen before it was embedded. In the case of the Ni-coated FBG sensor embedded by using automatic TIG welding, the thermal sensitivity obtained after the embedding process is higher than that observed previously. However, for the Cu-coated FBG sensors, the thermal sensitivity obtained after both embedding processes is lower than was seen for the previous process with the results being very close to each other. After the coated FBG sensors are embedded, the thermal sensitivity changes, because

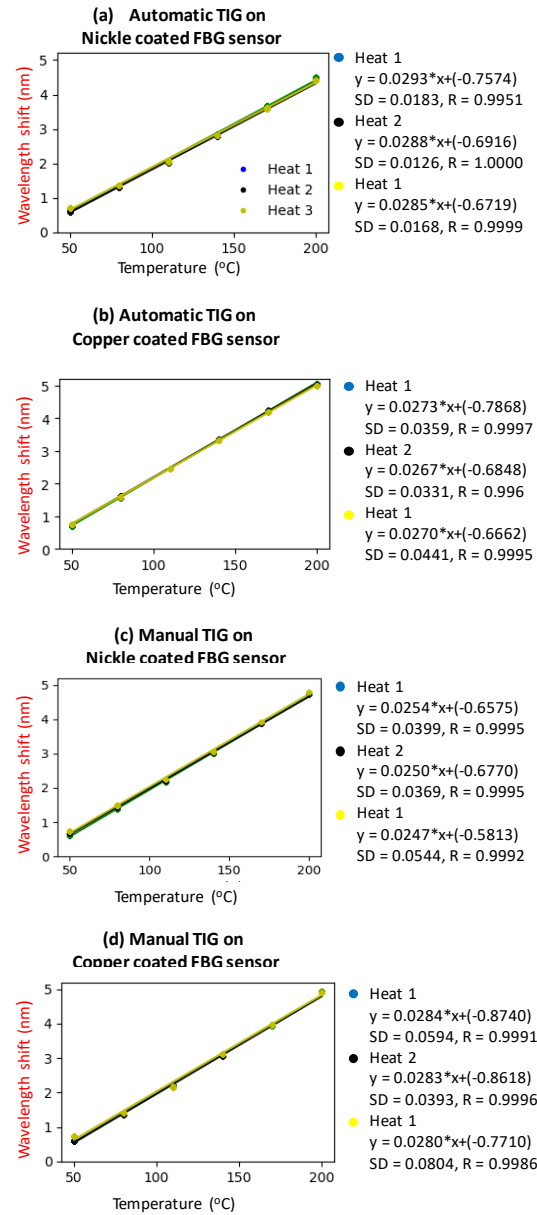


Fig. 6. Results of the calibration after the temperature tests on the embedded FBGs for (a) automatic TIG on a nickel-coated FBG, (b) automatic TIG on a copper-coated FBG, (c) manual TIG on a nickel-coated FBG and (d) manual TIG on a copper-coated FBG.

this depends of the embedding depth in the sample of each sensor and because of the thermal conductivity of the sensor coating used. In Table II, the embedding depth for each FBG sensor is shown. In the case of the Cu-coated FBG sensors, the

TABLE II
SENSITIVITIES ACHIEVED BEFORE AND AFTER EMBEDDING THE FBGS

Embedding process	Coating material	Average Diameter before embedding (μm)	Embedding depth (mm)	Embedding length (mm)	Sensitivity before embedding ($\text{nm}/^\circ\text{C}$)	Sensitivity after embedding ($\text{nm}/^\circ\text{C}$)
Automatic TIG	Nickel	464	1.4	26	0.024	0.029
	Copper	592	1.2	46	0.032	0.027
Manual TIG	Nickel	526	1.2	20	0.025	0.025
	Copper	738	1.3	17	0.034	0.028

thermal sensitivity is very close because the embedding depth is also very similar. However, in the case of the Ni-coated FBG sensors, the depth is higher for the Ni-coated FBG sensor embedded by using the Automatic TIG welding process, which causes the thermal sensitivity of this sensor to be higher than in the case of the Ni-coated FBG sensor embedded by use of the manual TIG welding process. Moreover, the thermal response for the Cu-coated FBG sensors embedded by use of the manual TIG welding process is repeatable and the sensitivity obtained is in accordance with that of the other FBG-embedded sensors and with the embedding depth used.

3) Tensile tests

In the strain calibration undertaken, three repetitions of the tensile tests were undertaken over the range from 0 to 30kN, in steps of 5kN, and performed for each specimen of the embedded sensor, as depicted in Fig. 7. In all three cases, the first of these tests shows a greater level of instability. This effect has already been discussed in the literature and is attributed to the residual strains remaining from the embedding process, which cause the FBG to settle during the first applications of the loading [1]. In the tests performed and reported in this work, it can also be seen that there is slippage of the specimen in the tensile test machine, the effect of which is depicted in Fig. 8(a), since the strain gage shown in Fig. 8(a) also shows a settling effect. Other than that, the responses are linear with load and strain, as can be seen in Fig. 9, where the calibration of the FBG sensor (compared to that from a conventional strain gage) has been performed and results reported. The sensitivities obtained from the data in Fig. 9, as detailed in Table III, range from 0.0010 nm/ $\mu\epsilon$ to 0.0012nm/ $\mu\epsilon$ in the cases of the automatic TIG embedding and the nickel-coated manual TIG embedding. These results are in good agreement with those reported in previous studies [5] and are in accordance with the original FBG sensitivities i.e. those before coating and embedding. In the case of the copper-coated FBG embedded by using the manual TIG method, the sensitivity is very low at 0.0003nm/ $\mu\epsilon$. In Fig.7(d) and Fig.9 (d), the response of the embedded FBG sensor monitored during the tensile tests is shown. A small and noisy wavelength variation for each load step, compared with the rest of the embedded sensors, can be seen. This result can only be explained by there being a poor bond and damage to the spectrum caused during the embedding process (in the Spectral Analysis Section above, this is noted and indeed, in the following cross-section analysis

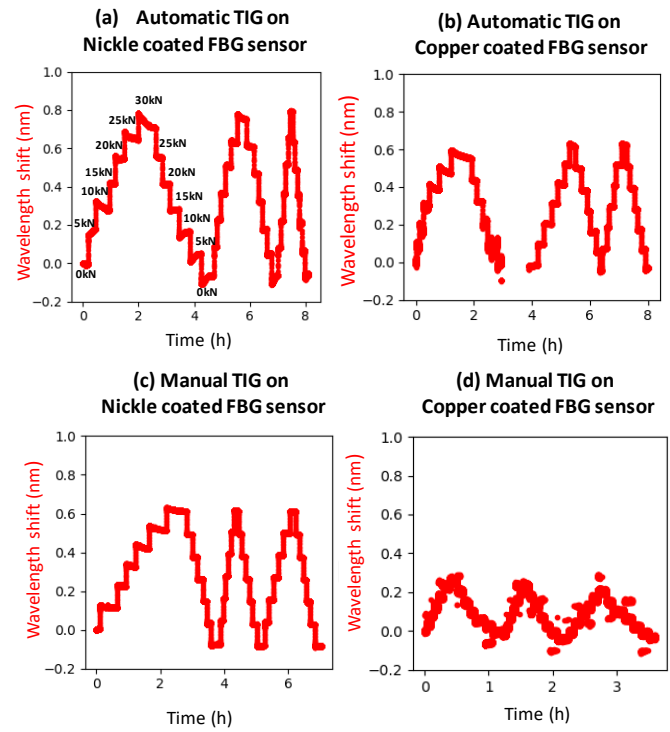


Fig. 7. Tensile tests of embedded FBGs for (a) automatic TIG on Nickel coated FBG, (b) automatic TIG on Copper coated FBG, (c) manual TIG on Nickel coated FBG and (d) manual TIG on Copper coated FBG.

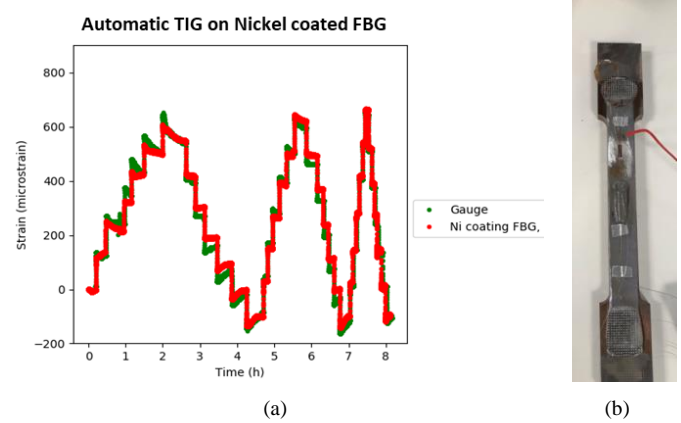


Fig. 8. Comparison of measurements of embedded FBG and strain gauge during tensile tests for automatic TIG on nickel-coated FBG (a), and photograph of the specimen with embedded FBG and strain gauge placement (b).

this effect is observed and explained more in detail). Further tests for manual TIG-embedded copper-coated FBGs have confirmed this behavior. A good adhesion during the embedding process is crucial in order to have a good strain response. An easy and non-destructive way to know if the FBG sensor is well embedded (by use of any of the welding techniques studied in this paper), and therefore will have a good strain response, is to see that the spectrum shows a symmetrical shape, without deformation or the presence of double peaks, for example.

4) Cross cut metallography

In the characterization of the specimens with embedded FBGs, one final analysis process was performed, this being done by analyzing the bond between the sensor, the coating and

TABLE III
COATED FBG DIAMETERS BEFORE AND AFTER EMBEDDING

Embedding process	Coating material	Average Diameter before embedding (μm)	Estimated sensitivity before embedding (nm/ $\mu\epsilon$)	Measured sensitivity after embedding (nm/ $\mu\epsilon$)
Automatic TIG	Nickel	464	0.0011	0.0012
	Copper	592	0.0011	0.0010
Manual TIG	Nickel	526	0.0011	0.0010
	Copper	738	0.0011	0.0003

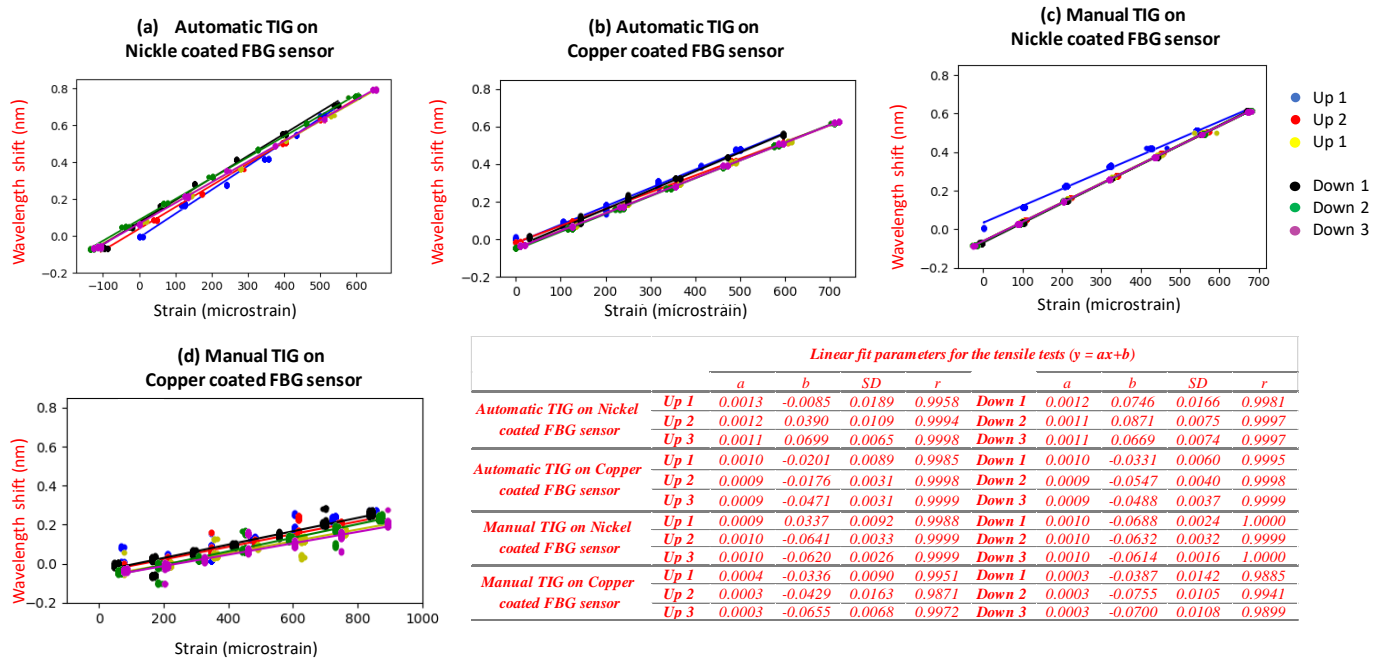


Fig. 9 Results of the calibration after the tensile tests on embedded FBGs for (a) automatic TIG on nickel-coated FBG, (b) automatic TIG on copper-coated FBG, (c) manual TIG on nickel-coated FBG and (d) manual TIG on copper-coated FBG. Up 1, 2 and 3 are for the cases where the strain is rising while Down 1, 2 and 3 are for the cases where the strain is falling.

the embedding metal with a crosscut metallography of each of the specimens, as shown in Fig. 10. The nickel-coated FBG, embedded by using the automatic TIG process and shown in Fig. 10(a), presents the best bond, and the nickel coating shows no damage, as it has kept its original shape and size of the coating. The copper-coated FBG embedded by use of the automatic TIG welding process, as seen in Fig. 10(b), has deteriorated more and in the bond between the copper and the tin alloy, intermetallic effects can be observed. In the case of the manual TIG embedded FBGs, both coatings have deteriorated, as presented in Fig. 10(c) and (d), especially for the case of the use of the copper coating. It should be noted that

the original diameter of the coated sensors, before and after the embedding process, is summarized in Table IV. The original shape of the coated optical fiber is not perfectly circular, because of the electroplating deposition technique used in its manufacture. The shape of the coated fiber is quasi-cylindrical, so any alteration to that implies damage to the coating by melting and generating intermetallic alloys. These changes in shape can be observed for both manual TIG embedded sensors, as was predicted in the previous sections. It can be seen from the strain calibration that the sensor showing the worst performance, the copper-coated FBG embedded by using the manual TIG process, is that with the severely damaged coating, this occurring during the embedding process. Thus, the embedding process clearly affects the performance of the sensors, with the coating being damaged. Despite this, for any of the embedded sensors, damage in the Au layer, in the cladding or in the core of the fibers is shown. The damage observed appears only in the outer metallic coating layer. The inner Cu and Ni layer (as well as the Au layer (Fig. 11)) do not show any disturbances or other defects, even after characterization temperature and strain tests have been performed.

TABLE IV
COATED FBG DIAMETERS BEFORE AND AFTER EMBEDDING

Embedding process	Coating material	Average Diameter before embedding (μm)	Diameter after embedding (μm)	
			Minimum	Maximum
Automatic TIG	Nickel	464	526	535
	Copper	592	564	567
Manual TIG	Nickel	526	388	480
	Copper	738	499	753

Fig. 10. Cross-section metallography of embedded FBGs for (a) automatic TIG on nickel-coated FBG, (b) automatic TIG on copper-coated FBG, (c) manual TIG on nickel-coated FBG and (d) manual TIG on copper-coated FBG.



Fig. 11. Detail of the cross-section metallography of embedded FBGs for automatic TIG on nickel-coated FBG.

IV. CONCLUSIONS

The potential of both manual and automatic TIG welding, as effective production techniques for the metal-embedding of FOS, has been successfully demonstrated for both nickel- and copper-coated FBGs. With both techniques and the coating materials considered, the sensitivity of the embedded FBGs is linear with temperature and strain and the sensors and fiber withstand the coating process. The nickel-coated FBG sensor, embedded using the automatic TIG process, shows the best

performance since the spectrum appearance is unchanged, the original sensitivity remains constant with strain and temperature and the cross-section metallography undertaken shows no damage to the coating. Copper-coated FBG sensors show more damage in the metallography results reported, especially in the case of the use of the manual TIG technique. The cross-section metallography results, in the latter case have shown how the coating is severely damaged with the use of this technique. This effect is also observed in the spectral analysis of this sensor after it having been embedded. This damage translates to a poorer performance of the sensor, as temperature and strain sensitivities are altered when compared with the original sensitivities of the coated sensors before embedding. It is therefore concluded that nickel-coated FBGs withstand the process better than copper-coated FBGs. Overall, although both techniques have been seen to be successful, the manual TIG process is more aggressive to the sensor than the automatic TIG approach, there being a tradeoff between the cost of the technique (lower for manual TIG welding) and the performance of the sensors (better for automatic TIG welding). Thus, with TIG welding being a widely available technique, inexpensive when compared to other high-power laser-based FOS metal embedding techniques, the results presented are important in choosing the best methods to use to ensure the widespread the use of embedded FOS in metals for diverse sensing applications.

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