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# **Wavelets based response spectrum compatible synthesis of accelerograms- Eurocode application (EC8)**

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## **Abstract**

An integrated approach for addressing the problem of synthesizing artificial seismic accelerograms compatible with a given displacement design/target spectrum is presented in conjunction with aseismic design applications. Initially, a stochastic dynamics solution is used to obtain a family of simulated non-stationary earthquake records whose response spectrum is on the average in good agreement with the target spectrum. The degree of the agreement depends significantly on the adoption of an appropriate parametric evolutionary power spectral form which is related to the target spectrum in an approximate manner. The performance of two commonly-used spectral forms along with a newly proposed one is assessed with respect to the elastic displacement design spectrum defined by the European code regulations (EC8).

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Subsequently, the computational versatility of the family of harmonic wavelets is employed to modify iteratively the simulated records to satisfy the compatibility criteria for artificial accelerograms prescribed by EC8. In the process, baseline correction steps, ordinarily taken to ensure that the obtained accelerograms are characterized by physically meaningful velocity and displacement traces, are elucidated. Obviously, the presented approach can be used not only in the case of the EC8, for which extensive numerical results/ examples are included, but also for any code provisions mandated by regulatory agencies. In any case, the presented numerical results can be quite useful in any aseismic design process dominated by the EC8 specifications.

**Keywords:** Response Spectrum; Stochastic Processes; Accelerograms; Evolutionary Power Spectrum; Harmonic Wavelets; Eurocode 8.

## 1. Introduction

Traditionally, code provisions for aseismic design of structures describe the seismic severity by means of smooth design (response) elastic and inelastic spectra. This practice facilitates significantly the design of regular structures in the framework of equivalent linear static or dynamic analysis incorporating proper modal combination rules. However, aseismic code regulations prescribe additional linear and/or non-linear dynamic time-history analyses to be performed for the design of facilities of critical importance and of structures incorporating non-conventional means of protection against the seismic hazard (e.g. seismic isolation, energy dissipation devices, tuned-mass dampers e.t.c.). In these cases, the input seismic action is represented by a suite of “real”

recorded earthquake accelerograms associated with historical seismic events or by an ensemble of numerically simulated earthquake signals. Typically, the response spectra of the adopted time-histories must satisfy certain criteria of compatibility with the elastic design spectra.

There are several factors likely to contribute to the extensive use of time-integration analyses for the mitigation of the seismic hazard in the built environment in the near future. These include the availability of more powerful computers, the increased capabilities of commercial software to account for potential inelastic behavior of structural systems, the need for constructing ever more sophisticated structured facilities (e.g. base isolated structures, nuclear power plants e.t.c.), and for upgrading/retrofitting the important/damaged existing ones. In this context, the development of dependable tools to make readily available realistic design spectrum compatible seismic accelerograms satisfying the related aseismic code provisions to practitioners is quite pertinent.

Most of the early methods for the generation of response spectrum compatible earthquake records are cited in the review articles of Ahmadi [1], and Spanos [2]. More recent commonly-used methods for the purpose are described in the studies of Preumont [3], Naeim and Lew [4], and Carballo and Cornell [5].

Lately, the problem at hand has been addressed by several researchers using various non-traditional in the field of structural dynamics techniques. Wang et al. [6] processed a collection of real accelerograms via the adaptive chirplet transform to reach a joint time-frequency representation of the signals. Similarly, Wen and Gu [7] utilized the empirical mode decomposition algorithm in cascade with the Hilbert transform to derive

an alternative time-frequency representation of individual accelerograms. In both of these studies, the derived representations were used in conjunction with a common random field simulation method to produce artificial seismic records possessing frequency content and response spectra of similar characteristics to those attained by the original recorded signals. Gupta and Joshi [8] and Shrinkhade and Gupta [9] cast the problem on a purely stochastic basis by deriving response spectrum consistent power spectra. Then, the phase characteristics of certain real accelerograms were used to introduce non-stationary attributes in the generated artificial time-histories. Conte and Peng [10] obtained similar results by considering a time-dependent (evolutionary) power spectrum numerically estimated by individual real acceleration time-histories. Subsequently, non-stationary artificial accelerograms compatible with this evolutionary power spectrum were produced by way of a special adaptive least-square fitting scheme. Lin and Ghaboussi [11] considered a relatively large ensemble of real accelerograms to “train” an appropriately constructed stochastic neural network. Hence, the trained network was used to generate artificial signals of comparable spectral and waveform characteristics with those of the ensemble accelerograms given a design spectrum as input.

From a deterministic viewpoint, Karabalis et al. [12] incorporated certain numerical schemes to appropriately modify individual recorded accelerograms so that their response spectra are in close agreement with a given design spectrum. Mukherjee and Gupta [13] and Hancock et al. [14] employed wavelet-based methods in the frequency and in the time domain, respectively, for the same purpose. A considerably different approach was proposed by Naeim et al. [15], incorporating a specific genetic algorithm to select and scale in the time domain a proper subset of recorded

accelerograms out of a large databank obeying to certain design spectrum compatibility criteria.

Obviously, in the preceding methods and in most of other ones proposed in the literature, a suite of real seismic accelerograms is assumed to be available to the designer. Ideally, it should include strong ground motion time histories recorded under certain soil conditions and seismological environments related to the design spectrum with which compatibility is ultimately pursued. Even though databases of recorded accelerograms are being gradually extended, the formation of such a suite of signals may not be readily feasible for specific seismically active regions. For instance, in some cases, such databases contain incomplete background information about the provided signals. Furthermore, the regulatory agencies may only provide a very “loose” classification of soil types, while typically no detailed information is included about the seismogenetic features of the source(s) considered in the definition of the design spectrum.

To circumvent the above requirement and the limitations of the deterministic methods, a stochastic approach originally established in Spanos and Vargas Loli [16], is followed in this paper to obtain ensembles of seismic records whose average response spectrum bears close resemblance with a given design (response) spectrum. It should be noted that this approach accounts for the non-stationarity of the generated signals in a more direct manner than in the previous studies of Gupta and Joshi [8], and Shrinikade and Gupta [9]. In particular, a simulated earthquake accelerogram is construed as a sample of a non-stationary zero-mean random process characterized by an analytically defined uniformly modulated evolutionary power spectrum (EPS) [17]. The latter spectrum is related to the design spectrum through an approximate formula involving the

maximum variance of the amplitude of the response of a single-degree-of-freedom oscillator to a non-stationary stochastic excitation. An appropriate minimization problem is formulated and solved numerically to determine the requisite parameters defining the EPS. Upon determination of the EPS, an auto-regressive-moving-average model is employed to simulate non-stationary artificial accelerograms compatible with the EPS [18]. The obtained signals are then individually modified by means of the harmonic wavelet transform [19, 20], in the context of an iterative scheme [13], to improve the agreement of their response spectra with the target design spectrum. It is noted that the unique attributes of the generalized harmonic wavelets provide enhanced flexibility in the representation of signals throughout the frequency domain which enhances significantly the efficiency of the original matching procedure of Mukherjee and Gupta [13]. In the process, an efficient baseline correction technique is utilized [21] to yield accelerograms possessing physically proper velocity and displacement traces.

The proposed methodology encompasses two distinct formulations: the stochastic formulation where an appropriate EPS must be defined and the iterative matching formulation whose efficiency depends on the construction of the harmonic wavelet basis functions. Both of these formulations are extended and/or customized with respect to the elastic displacement design spectrum, and the corresponding compatibility criteria for artificial accelerograms set forth by the European aseismic code provisions (EC8) [22]. Nevertheless, adopting the specific code provisions does not limit the applicability of the proposed methodology; it only exemplifies its versatility.

To this end, the potential of three different spectral forms of exponentially modulated in time power spectra is assessed for the specification of the aforementioned



EPS: the Kanai-Tajimi [23], the Clough-Penzien [24], and a novel one comprising a predefined high-pass Butterworth filter (e.g. [25]) in series with the Kanai-Tajimi spectrum. Furthermore, the construction of custom case-dependent harmonic wavelet basis with scales of non-uniform width in the frequency domain is adopted to satisfy efficiently the compatibility criteria mandated by the EC8.

## 2. Stochastic simulation of spectrum compatible artificial earthquake records

In this section, the pertinent theoretical background for associating an evolutionary power spectrum with a given displacement response (design) spectrum is first reviewed. Special attention is given to the analytical spectral form characterizing the stationary part of this evolutionary power spectrum and alternative expressions are considered for the purpose. A brief presentation of an efficient filtering method for generating non-stationary signals being samples of an underlying evolutionary power spectrum is also included.

### 2.1. Formulation of the simulation problem on a stochastic basis

Let the ground acceleration  $u_g(t)$  due to a seismic event be modeled as a realization of a zero-mean separable non-stationary stochastic process expressed in the domain of time  $t$  by the equation

$$u_g(t) = A(t)y(t), \quad (1)$$

where  $A(t)$  is assumed to be a slowly-varying time-dependent envelop function that modulates a zero-mean stationary stochastic process  $y(t)$ . The associated two-sided

evolutionary power spectrum  $S(t, \omega)$  of the non-stationary process is expressed in the frequency ( $\omega$ ) domain as [17]

$$S(t, \omega) = |A(t)|^2 S(\omega), \quad (2)$$

where  $S(\omega)$  is the two-sided power spectrum of the stationary process  $y(t)$ .

Consider a unit-mass linear single-degree-of-freedom (SDOF) quiescent oscillator with ratio of critical damping  $\zeta$  and natural frequency  $\omega_n$ , base-excited by the process  $u_g(t)$ . The motion of this system is governed by the equation

$$\begin{aligned} \ddot{x}(t) + 2\zeta\omega_n\dot{x}(t) + \omega_n^2x(t) &= -u_g(t) \\ x(0) = \dot{x}(0) &= 0 \end{aligned}, \quad (3)$$

in which  $x(t)$  is the displacement trace of the oscillator relative to the motion of the ground and the dot over a symbol denotes differentiation with respect to time.

Assuming that the input energy, as expressed by  $S(t, \omega)$ , is distributed over a broad frequency band throughout the duration of the process  $u_g(t)$ , it can be argued that the response of lightly damped oscillators ( $\zeta \ll 1$ ) trails a pseudo-sinusoidal motion. That is:

$$x(t) = a(t) \cos[\omega_n t + \varphi(t)], \quad (4)$$

where  $a(t)$  and  $\varphi(t)$ , are the response amplitude and phase and correspond to processes of slow temporal evolution statistics.

The aforementioned assumptions are common in the field of random vibrations (see e.g. [26]), and reflect the fact that SDOF systems with small ratio of critical damping attain highly resonant transfer functions centered at the natural frequency ( $\omega_n$ ). Therefore, these systems act as pass-band filters when excited by relatively broadband input, as is usually the case of earthquake induced strong ground motions, and thus their response is

dominated by the frequencies close to  $\omega_n$ . Under these assumptions, it can be shown that the probability density function of the response amplitude follows a time-dependent Rayleigh distribution [27]

$$p(a, t) = \frac{a}{\sigma_a^2(t)} \exp\left(\frac{-a^2}{2\sigma_a^2(t)}\right), \quad (5)$$

where the function  $\sigma_a^2(t)$  is the variance of the amplitude given by the equation

$$\sigma_a^2(t) = \frac{\pi}{\omega_n^2} \exp(-2\zeta\omega_n t) \int_0^t \exp(2\zeta\omega_n \tau) S(\tau, \omega_n) d\tau. \quad (6)$$

To this end, a straightforward relation between a given (target) displacement design spectrum  $S_d(\omega_n, \zeta)$  and the evolutionary power spectrum of Eq. (2) can be established through the maximum value of the variance of the response amplitude [16]:

$$S_d(\omega_n, \zeta) = r \max \{ \sigma_a(\omega_n, \zeta) \}, \quad (7)$$

where  $r$  is known as the “peak factor” [28]. In general,  $r$  depends on the stiffness ( $\omega_n$ ), and damping ( $\zeta$ ) of the SDOF oscillator, on the frequency content and duration of the input process  $u_g(t)$ , and on the level of uncertainty furnished by the design spectrum as specified by regulatory agencies. The exact determination of the peak factor requires the solution of the first-passage problem which is mathematically intractable, especially for non-stationary input processes. It is pointed out that for stationary input processes some reliable approximate formulae for estimating the peak factor exist in the literature (e.g. [29], [30]). However, the use of such formulae for the determination of  $r$  in the case considered herein necessitates replacing the non-stationary process of Eq. (1) by an equivalent stationary process of reduced duration [28]: an assumption which is not absolutely consistent with the objective of defining a design spectrum compatible non-

stationary process. Therefore, for the purposes of the present study,  $r$  will be treated as a constant. Additional comments on selecting an appropriate value for the peak factor are given in section 4 incorporating new numerical results pertaining to the EC8 displacement design spectrum [22].

## *2.2 Spectral form of the evolutionary power spectrum*

In pursuing a solution to the simulation problem defined by Eq. (7), appropriate analytical expressions for the modulation function  $A(t)$  and the power spectrum  $S(\omega)$  must be adopted. These must be compatible with the assumptions made in deriving Eqs. (5) and (6) and should capture adequately the physical aspects of the problem.

In this regard, the Bogdanoff-Golberg-Bernard (BGB) envelope function defined by [31]

$$A(t) = Ct \exp\left(-\frac{b}{2}t\right) \quad (8)$$

is used, where  $C > 0$  and  $0 < b < 1$  are parameters to be determined. This function accommodates appropriately the time-evolving intensity typically exhibited by recorded seismic accelerograms; namely, a decaying segment preceded by a short initial period of development. Note that the value of  $C$  is proportional to the peak ground acceleration, while the parameter  $b$  controls the shape of the envelope and thus the effective duration of the strong ground motion. Recently, the “slowly-varying” feature of the BGB function, which must hold for Eq. (2) to be valid, was ascertained by means of the adaptive chirplet decomposition for an assumed value of  $b = 0.50$  [32]. Furthermore, the spectral form considered for the stationary part of the process  $u_g(t)$  reads

$$S(\omega) = G(\omega) \frac{1 + 4\zeta_g^2 \left(\frac{\omega}{\omega_g}\right)^2}{\left(1 - \left(\frac{\omega}{\omega_g}\right)^2\right)^2 + 4\zeta_g^2 \left(\frac{\omega}{\omega_g}\right)^2}; |\omega| \leq \omega_b, \quad (9)$$

in which  $\omega_g$  and  $\zeta_g$  are positive parameters and  $\omega_b$  signifies the highest frequency of interest.

Setting  $G(\omega) = 1$  in Eq. (9) yields the well-known Kanai-Tajimi (KT) spectrum [23]. Apart from its simplicity, the main asset of the KT spectrum is that it lends itself to a clear physical interpretation associated with site specific soil conditions. In particular, it accounts for the resonant filtering effects that the surface soil deposits have on propagating seismic waves by a linear SDOF system with natural frequency  $\omega_g$  and damping ratio  $\zeta_g$ . In this context, it has been extensively used in the past in random vibration analysis of structures (e.g. [28], [29]), and in strong ground motion characterization (e.g. [33]). Nevertheless, the KT filter has the major disadvantage of allowing for the presence of non-negligible low frequency content in the spectral representation of the acceleration process  $u_g(t)$ . Such low frequency components are considerably accentuated upon integration of the accelerograms and have a significant impact to their corresponding displacement traces. Specifically, this leads to displacement time-histories exhibiting a monotonically increasing trend and yielding unrealistically high permanent deformations similar to those reported in [4].

The Clough-Penzien (CP) spectral form incorporates a second order high-pass filter to suppress the low frequency content allowed by the KT spectrum [24]. It is obtained by setting

$$G(\omega) = \frac{\left(\frac{\omega}{\omega_f}\right)^4}{\left(1 - \left(\frac{\omega}{\omega_f}\right)^2\right)^2 + 4\zeta_f^2 \left(\frac{\omega}{\omega_f}\right)^2}, \quad (10)$$

in Eq. (9), where  $\omega_f$  and  $\zeta_f$  are positive parameters related with the cut-off frequency and the steepness of the transfer function of the high-pass filter  $G(\omega)$ . It is reasonable to attribute physical meaning to Eq. (10), since it coincides with the transfer function of a SDOF system with natural frequency  $\omega_f$  and damping ratio  $\zeta_f$ , and is used in series with the KT filter. Indeed, some researchers have argued that  $\omega_f$  and  $\zeta_f$  can be interpreted as the stiffness and damping ratio of the geological formations of the crust of the Earth, the bedrock (e.g. [34]). Nevertheless, the filter of Eq. (10) is primarily a signal processing element, and thus, the values of parameters  $\omega_f$  and  $\zeta_f$  should be set appropriately to eliminate the spurious low frequencies [24]. In any case, note that by adopting the CP spectral form the complexity of the simulation problem is significantly increased since four more undetermined parameters are additionally introduced to the required parameters, two, for the definition of the BGB modulating envelop. In this respect, it is proposed to utilize a predefined standard infinite impulse response high-pass filter in cascade with the KT band-pass filter. For instance, a Butterworth filter given by the equation [25]

$$G(\omega) = \frac{\omega^{2N}}{\omega^{2N} + \omega_o^{2N}} \quad (11)$$

can be assumed in Eq. (9), where  $N$  and  $\omega_o$  denote the filter order and cut-off frequency, respectively. These quantities can be judiciously selected so that adequate filtering of the low frequencies is achieved, while the design of the high-pass filter part  $G(\omega)$  is left out

of the simulation problem. Further elucidating comments on the various spectral forms presented in this section are given in light of numerical results in section 4.1.

### 2.3 Approximate solution of the simulation problem

Combining Eqs. (2), (6), and (8) the following expression for the time-dependent variance of the response amplitude is obtained

$$\sigma_a^2(t) = \frac{\pi C^2}{\omega_n^2 \gamma^3} \left\{ \gamma^2 t^2 \exp(-bt) - 2\gamma t \exp(-bt) + 2 \exp(-bt) - 2 \exp(-2\zeta \omega_n t) \right\}, \quad (12)$$

where

$$\gamma = 2\zeta \omega_n - b. \quad (13)$$

This expression possesses a global maximum at time  $t=t^*$ . This time instant can be determined by setting the first time derivative of Eq. (12) equal to zero. This criterion leads to the condition

$$\gamma^2 (2t^* - bt^{*2}) - 2\gamma (1 - bt^*) - 2b + 4\zeta \omega_n \exp(-\gamma t^*) = 0. \quad (14)$$

Application of the previous operation in Eq. (6), and use of Eqs. (2) and (8) yields the maximum value of the variance of the response amplitude. That is,

$$\max \left\{ \sigma_a(\omega_n, \zeta) \right\} = \frac{\pi C^2 t^{*2} \exp(-bt^*)}{2\zeta \omega_n^3} S(\omega_n). \quad (15)$$

An approximate solution to the simulation problem defined by Eqs. (7), (14), and (15) is next pursued, as it has been proposed in [16]. In this regard, it is sought to satisfy approximately Eq. (7) in a point-wise manner, at a certain set of frequencies  $\{\omega_{n(j)}\}$  for  $j=1, \dots, M$ , in the least square sense. This leads to a least squares minimization problem which can be cast as

$$\min \left\{ \sum_{j=1}^{2M} (S_j - \sigma_j)^2 \right\}, \quad (16)$$

where

$$S_j = \begin{cases} S_d^2(\omega_{n(j)}, \zeta), & j = 1, \dots, M \\ 0, & j = M+1, \dots, 2M \end{cases}, \quad (17)$$

and

$$\sigma_j = \begin{cases} \frac{r^2 C^2 t_j^{*2} \exp(-bt_j^*)}{2\zeta \omega_{n(j)}^3} S(\omega_{n(j)}), & j = 1, \dots, M \\ \gamma_{j-M}^2 (2t_{j-M}^* - bt_{j-M}^{*2}) - 2\gamma_{j-M} (1 - bt_{j-M}^*) - \\ - 2b + 4\zeta \omega_{n(j-M)} \exp(-\gamma_{j-M} t_{j-M}^*), & j = M+1, \dots, 2M \end{cases} \quad (18)$$

In Eqs. (16)-(18) the unknowns to be determined are the set of  $M$  time instants  $\{t_k^*\}$ ,  $C$ ,  $b$ , plus all necessary parameters involved in the analytical expression of  $S(\omega)$ , while the number of equations is  $2M$ . In practice, the number of equations will always be greater than the total number of unknowns, since for an acceptable approximation to the solution of the problem considered several tenths of points  $\{\omega_{n(j)}\}$  along the frequency band of concern should be included. Thus, Eqs. (16)-(18) define a typical high-dimensional over-determined non-linear least-square fit optimization problem. In this study, a Levenberg-Marquardt algorithm with line search is utilized to numerically solve this problem (see e.g. [35]).

#### 2.4 Generation of artificial non-stationary earthquake records

Upon solving the optimization problem of Eq. (16), the complete definition for the evolutionary power spectrum  $S(t, \omega)$  is accomplished. Then, an appropriate random



field simulation technique can be employed to synthesize an arbitrarily large number of non-stationary accelerograms as realizations of the process characterized by  $S(t, \omega)$ . In the case of the uniformly modulated non-stationary stochastic processes, this task can be carried out conveniently in two steps: First, stationary time histories  $y(t)$  compatible with a specific power spectrum  $S(\omega)$  are generated. Next, the corresponding non-stationary time-histories are obtained by multiplying the stationary records with the envelop function  $A(t)$ , as Eq. (1) suggests. A plethora of techniques for synthesizing power spectrum compatible stationary signals exist in the literature. A self-contained exposition of the topic presenting the most common of the methods is provided in [18].

In this study, the so-called ARMA simulation method is used. Specifically, a discrete stationary stochastic process  $\tilde{y}$  is generated as the response of a linear time-invariant autoregressive moving average (ARMA) digital filter subject to clipped white noise excitation [36]. The  $s$ -sample of an ARMA( $p, q$ ) process is calculated recursively as a linear combination of the previous  $p$  samples plus a convolution term as follows

$$\tilde{y}[s] = -\sum_{k=1}^p b_k \tilde{y}[s-k] + \sum_{l=0}^q c_l w[r-l], \quad (19)$$

where the  $b_k$  and  $c_l$  are the coefficients of the ARMA filter. The symbol  $w$  denotes a discrete white noise process band-limited to  $\omega_b$  defined by the autocorrelation function

$$E\{w[u]w[v]\} = 2\omega_b \delta_{uv}. \quad (20)$$

In this equation  $E\{\cdot\}$  denotes the operator of mathematical expectation, and  $\delta_{uv}$  is the Kronecker delta. Intuitively, the objective in this procedure is to “color” the latter process via the ARMA filter so that the filtered process is characterized by the given power spectrum  $S(\omega)$ . In mathematical terms this translates into determining the coefficients  $b_k$

and  $c_l$  such that the squared modulus of the frequency response of the ARMA filter matches the power spectrum  $S(\omega)$ . Specifically, require that

$$S(\omega) = \left| H(e^{i\omega T_s}) \right|^2. \quad (21)$$

In Eq. (21)  $T_s$  is the sampling period of the discrete process which must comply with the Nyquist condition to avoid aliasing. That is,

$$T_s \leq \frac{\pi}{\omega_b}. \quad (22)$$

Further,  $H$  denotes the transfer function of the ARMA filter which can be expressed as

$$H(e^{i\omega T_s}) = \frac{\sum_{l=0}^q c_l e^{-li\omega T_s}}{1 + \sum_{k=1}^p b_k e^{-ki\omega T_s}}. \quad (23)$$

In the ensuing analysis the auto/cross-correlation matching (ACM) procedure is used to determine the filter coefficients. In implementing this scheme, linear prediction theory used in system identification is used to construct a relatively long autoregressive (AR) digital filter to represent  $S(\omega)$  as a first approximation. Next, the output auto-correlation and the input/output cross-correlation sequences between this preliminary AR and the final ARMA model are equated. Eventually, the coefficients of the ARMA filter are calculated by solving a  $p+q$  by  $p+q$  system of linear equations. The mathematical details of the ACM procedure can be found in [18].

### **3. Enhanced response spectrum matching of synthesized records using the Harmonic Wavelet Transform**

Obviously, the previously described procedure cannot guarantee that the response spectrum of the individual synthetic signals produced will match exactly the target design spectrum and satisfy the usual criteria for artificial accelerograms mandated by regulatory agencies (see e.g. [22]). This is because of the various assumptions involved in the formulation of the simulation problem, the approximate manner by which a solution to this problem is sought, and the statistical nature characterizing the generation of the signals by way of random field simulation.

Nevertheless, any arbitrary seismic accelerogram, whether artificial or recorded, can be appropriately modified to improve the agreement of its response spectrum with the target design spectrum. For this purpose, the generalized harmonic wavelets [19, 20] are utilized herein for processing the generated accelerograms along with an iterative matching procedure originally proposed in [13]. Compared to the modified Littlewood-Pauley basis functions considered in [13], the generalized harmonic wavelets provide a more flexible and balanced representation of signals throughout the frequency domain [20]. Furthermore, advantage is taken of an efficient algorithm incorporating the Fast Fourier Transform for the signal decomposition and reconstruction [37]. These attributes render the Harmonic wavelet transform an effective tool for processing signals to achieve enhanced response spectrum matching as will be shown in the ensuing numerical results. This objective is achieved herein by an iterative numerical procedure combined with an appropriate high-pass filtering method for the requisite baseline adjustments.

### 3.1 The Harmonic Wavelet Transform

Generalized harmonic wavelets have a box-shaped band-limited spectrum. A wavelet of  $(m,n)$  scale and  $k$  position in time is represented in the frequency domain by the equation [19]

$$\Psi_{m,n}(\omega) = \begin{cases} \frac{1}{(n-m)\Delta\omega} \exp\left(\frac{-i\omega k T_o}{(n-m)}\right), & m\Delta\omega \leq \omega \leq n\Delta\omega, \\ 0, & \text{otherwise} \end{cases}, \quad (24)$$

where  $m$ ,  $n$ , and  $k$  are taken to be positive integer numbers in what follows and

$$\Delta\omega = \frac{2\pi}{T_o}, \quad (25)$$

with  $T_o$  being the total length of the time interval considered (i.e. the duration of the signals generated by Eq. (20)), in seconds. The time-domain Fourier Transform pair of Eq. (25) is complex-valued [20], with magnitude

$$|\psi_{(m,n),k}(t)| = \frac{\sin\left(\pi\left(\frac{t}{T_o} - \frac{k}{n-m}\right)(n-m)\right)}{\pi\left(\frac{t}{T_o} - \frac{k}{n-m}\right)(n-m)}, \quad (26)$$

and phase

$$\varphi_{(m,n),k}(t) = \pi\left(\frac{t}{T_o} - \frac{k}{n-m}\right)(m+n). \quad (27)$$

It has been proved [19] that a collection of harmonic wavelets spanning adjacent non-overlapping intervals at different scales along the frequency axis, as shown schematically in Fig. 1, forms a complete orthogonal basis. Then, the pertinent continuous Harmonic Wavelet Transform (HWT) [19]

$$[W_\psi f](m, n, k) = \frac{n-m}{T_o} \int_{-\infty}^{\infty} f(t) \overline{\psi_{(m,n),k}(t)} dt, \quad (28)$$

projects any finite energy signal  $f(t)$  on this basis function. In Eq. (28) the bar over a symbol stands for complex conjugation. It is emphasized that the orthogonal property of the harmonic wavelet basis allows for a perfect reconstruction of the original signal given its HWT, and is associated with energy preservation concepts.

### 3.2 Iterative matching scheme

It can be deduced by the preceding exposition that the HWT decomposes a real signal  $f(t)$  into several sub-signals  $f_{m,n}(t)$ , each one of them corresponding to a certain band of frequencies defined by the  $(m,n)$  pair, so that [20]

$$f(t) = \sum_{m,n} f_{m,n}(t), \quad (29)$$

where

$$f_{m,n}(t) = 2 \operatorname{Re} \left\{ \sum_{k=0}^{n-m-1} [W_\psi f](m, n, k) \psi_{(m,n),k}(t) \right\}. \quad (30)$$

Taking into consideration the discussions of section 2.1 concerning the shape of the transfer function of lightly damped SDOF oscillators, it can be argued that a specific part  $f_{m_j, n_j}(t)$  of the original signal  $f(t)$  will mainly influence the response of those SDOF oscillators whose natural frequencies fall within the interval  $[m_j \Delta \omega, n_j \Delta \omega]$ . Thus, an iterative modification procedure can be devised to improve the matching of the displacement response spectrum of an accelerogram  $f(t)$  with a target spectrum  $S_d$  [13]. At the  $v$ -th iteration all sub-signals are scaled according to the equation

$$f_{m,n}^{(v+1)}(t) = f_{m,n}^{(v)}(t) \frac{\int_{m\Delta\omega}^{n\Delta\omega} S_d(\omega) d\omega}{\int_{m\Delta\omega}^{n\Delta\omega} D^{(v)}(\omega) d\omega}, \quad (31)$$

where  $D^{(v)}(T)$  is the displacement response spectrum related to  $f^{(v)}(t)$  which is obtained by Eq. (29). Note that a sufficient number of properly defined  $(m,n)$  pairs should be used to cover all frequencies of interest. Furthermore, the width  $(n-m)\Delta\omega$  of the various pairs can be arbitrarily small and varying among different scales, as illustrated in Fig. 1 for a given duration  $T_o$ . This yields a significant advantage over the modified Littlewood-Pauley basis which defines intervals of logarithmically increasing width on the frequency domain as it proceeds towards the higher frequencies [13]. Numerical evidence, and additional comments on this feature of the harmonic wavelets in practical terms are provided in sections 4.3 and 4.4.

### 3.3 Baseline correction considerations

Artificial seismic accelerograms to be used in the earthquake resistant design of structures require that certain baseline corrections must be performed as in the case of any recorded accelerogram [38]. This requirement has been reported and addressed by several researchers in the past (e.g. [4], [12], [13]). It stems from the need to produce accelerograms yielding realistic displacement traces. To this end, processing of the accelerograms with a Butterworth high-pass filter of order 4 and cut-off frequency of 0.10Hz is employed in this study to acquire baseline corrected accelerograms. Anti-causal zero-phase filtering is carried out. That is, the accelerogram is filtered once by the aforementioned filter in the forward direction; then the filtered signal is reversed in time

and passes through the same filter again. In this manner, no phase distortion takes place, and thus the properties of the filter considered have minimum impact on both the shape of the displacement time-histories and the long period displacement spectral ordinates [39]. Appropriate zero-padding before the initiation and at the end of the accelerograms is performed before applying the anti-causal filter [40]. These pads are retained throughout the integrations to construct compatible suites of acceleration, velocity and displacement records [41].

#### **4. Application to the Eurocode 8 design spectrum**

This section provides numerical results pertaining to the displacement design spectrum prescribed by the European aseismic code provisions (EC8) given in Appendix A. In this context, an estimate for the value of the peak factor which yields a better matching of the average response spectra of simulated accelerograms with the target spectrum is proposed. Furthermore, an assessment of the three spectral forms of section 2.2 is included. The performance of the harmonic wavelet-based iterative scheme is also demonstrated using a single simulated signal. Lastly, it is shown how to take advantage of the versatility of the generalized harmonic wavelet basis to satisfy the compatibility criteria for artificial accelerograms mandated by the EC8.

##### *4.1 Selection of the peak factor $r$*

Taking into account the stochastic structure of the response envelop  $a(t)$  (see Eq. (5)), it is a reasonable from a theoretical viewpoint to equate the peak factor  $r$  of Eq. (7)

to the ratio of the maximum mean ( $\mu$ ) over the maximum standard deviation ( $\sigma$ ) for Rayleigh distribution. That is, [16]

$$r = \frac{\max\{\mu_a\}}{\max\{\sigma_a\}} = \sqrt{\frac{\pi}{2}}. \quad (32)$$

However, extensive numerical experimentation (Monte Carlo simulations), not included here for brevity, pertaining to the EC8 design spectrum has shown that adopting the above value for  $r$  yield rather conservative results. In particular, the obtained response spectral ordinates of the simulated time-histories tend to be, on average, rather larger than the target ones for all natural periods considered. Notably, a similar trend is witnessed in the numerical results of the relevant research work by Spanos and Vargas Loli (1985) [16] for the case of the Newmark-Blume-Kapur and the Housner design spectra. In this respect, it is noted that the aforementioned numerical experiments have suggested that, at least in the case of the EC8 spectrum, adopting a peak factor 25% larger than that of Eq. (32) yields ensembles of artificial accelerograms whose average response spectra are close to the corresponding design spectra while a desirable level of conservatism is maintained. Thus, the latter value is the one adopted for  $r$  for all the ensuing numerical results included in this study.

#### *4.2 Assessment of various evolutionary power spectral forms*

Let the EC8 displacement design spectrum for soil conditions B, damping ratio  $\zeta=5\%$ , and peak ground acceleration (PGA) equal to 36% the acceleration of the gravity ( $g$ ) be the target spectrum (see also the Appendix A). The minimization problem set by Eq. (16) is solved for the three spectral forms defined in section 2.2. Namely the KT spectrum (Eq. (9) with  $G(\omega)=1$ ), the CP spectrum (Eqs. (9) and (10)), and the



Butterworth filtered Kanai-Tajimi (BWKT) spectrum (Eqs. (9) and (11)), modulated by the BGB envelop function (Eq. (8)) on an interval  $[T_{min}, T_{max}]$  of the axis of natural periods. The numerical values of the requisite parameters to defining the design spectrum compatible evolutionary power spectral forms under consideration are given in Table 1.

It is noted that in the BWKT case, the cut-off frequency  $\omega_o$  of the high-pass filter of Eq. (12) has been judiciously selected to coincide with the “corner” period  $T_D = 2\text{sec}$  (see Fig. (A1) of Appendix A), prior to the solution of Eqs. (16)-(18). Incidentally, the value of  $T_D$  is the same for all soil types [22], and thus the selected value for  $\omega_o$  is globally applicable. Should this specification change in future versions of the EC8, it is suggested to always set the cut-off frequency of the Butterworth filter equal to the corner period  $T_D$ ; extensive numerical testing has found this to be an effective choice. Moreover, the order of the Butterworth filter was set to  $N = 2$ , so that a meaningful comparison with the CP case to be possible.

It should be noted that for all soil conditions, the EC8 assumes that the maximum displacement of oscillators of natural period greater than 10 sec is independent of the stiffness of the oscillators, that is, it attains a constant value equal to the maximum displacement of the ground (see also Fig. A1 of Appendix A). Thus, extending the point-wise matching to periods beyond 10sec will not capture any additional physics to the optimization problem at hand. Hence, it is logical to assume  $T_{max} = 10\text{ sec}$ . In both the CP and BWKT cases of Table 1 excellent point-wise matching at 100 frequencies  $\omega_n$  has been achieved on the interval  $[0.63, 314.16]$  (rad/sec) which is mapped onto the interval  $[0.02(=T_{min}), 10(=T_{max})]$  (sec) on the axis of natural periods (Fig. 2). However, for the KT spectral form an attempt to extent the right limit of the matching interval ( $T_{max}$ ) to periods

greater than  $T_D = 2\text{sec}$  (i.e. to frequencies lower than  $3.14\text{ rad/sec}$ ) results in an unacceptably poor matching. An example is shown in Fig. 2 for  $T_{max} = 4\text{sec}$ . In fact, the optimization algorithm completely fails in the KT case for  $T_{max} > T_E$  ( $= 5\text{ sec}$  for soil B). This is because the KT spectrum does not incorporate enough “degrees of freedom” to effectively trace the given design spectrum in the region of relatively long periods. This aspect is interwoven with the incapability of the KT filter to effectively suppress the low frequencies as have been discussed to some extent in section 2.2. This disadvantage of the KT spectral form can also be inferred by Fig. 3 where plots of certain evolutionary power spectra of Table 1 are presented. In the same figure, it is observed that all spectra remain relatively broad throughout their effective duration and that their energy becomes negligible after 25 seconds.

Additional evolutionary CP power spectra compatible with EC8 design spectra for two different levels of intensity, and for all soil types defined in EC8 are included in Table 2. These results provide evidence that the values of the parameters yielded by the optimization solver are not numerical artifacts but actually reflect the physical aspects of the problem. Indeed, even though soil characterization is beyond the scope of the present study, it can be readily seen that the various soil conditions are represented by the power spectrum parameters. For instance, the value of  $\omega_g$  decreases while the damping ratio  $\zeta_g$  increases marching from stiff (i.e. type A) towards softer soil conditions (i.e. type D). More importantly, Table 2 can be used as an interpolation guide for assigning initial/seed values for the unknown parameters required by all common optimization algorithms for the solution of Eqs. (16)-(18); this is especially pertinent in case the use of a different PGA than those included in the table is mandated.

Three ensembles of 40 accelerograms, each compatible with the KT ( $T_{max}=2\text{sec}$ ), the BWKT, and the CP power spectra presented in Table 1 are synthesized using Eq. (19) and a discrete version of Eq. (1). The sampling interval has been taken equal to 0.01 sec to satisfy the condition of Eq. (22), and the duration of each record is 40sec. Baseline corrected versions of these records have been also produced using the methodology detailed in section 3.3. The average displacement response spectra for 5% damping of each of the ensembles are plotted in Figs. 4-6 for both the uncorrected (dotted lines) and the baseline corrected (solid lines) signals versus the target spectrum. In the same figures, the largest and smallest maximum displacement responses along with the medians are also shown versus the natural period of the oscillators considered to illustrate the statistical nature of the obtained spectral ordinates.

The fact that the KT spectrum does not filter the very low-frequency content in the acceleration traces causes difficulties in the corresponding displacement time-histories. This attribute ultimately affects the matching of the displacement response spectra with the target spectrum exhibiting undesirable trends as evidenced in Fig. (4). Clearly, the KT spectrum is not an optimal choice for the purpose. However, both the BWKT and the CP spectra yield satisfactory and practically similar results. Evidently, these spectra can be used interchangeably to shape the form of the evolutionary power spectrum of Eq. (2). To this end, note that the BWKT featuring the predefined high-pass Butterworth filter involves fewer free parameters to be determined. Furthermore, it is usually more convenient/ intuitive in practice to define a high-pass filter in signal processing terms; namely by selecting the properties of a typical IIR filter, versus selecting the stiffness and damping of a SDOF oscillator. In this regard, the newly

proposed BWKT filter may be more advantageous over the CP filter from a practical perspective.

#### *4.3 Performance of the iterative Harmonic Wavelet-based matching procedure*

In the context of the HWT, the efficiency of the iterative procedure outlined by Eq. (31) to modify a certain accelerogram for achieving a better matching of its response spectrum with a given design spectrum at all frequencies relies on the total number of the wavelet scales (bins of Fig. 1) considered. For a specific range of frequencies, and assuming uniform width for all scales, this number depends on the difference  $n-m$  (see Eq. (24)), and on the duration  $T_0$  of the accelerogram through the value of  $\Delta\omega$  (see Eq. (25)). Addressing the second dependence, it is a common practice in standard Fourier analysis to artificially augment the duration of a signal by adding zeros at the end of the record for obtaining a more adequate representation of the original signal in the frequency domain. This technique can be used herein to obtain a smaller value of  $\Delta\omega$  which eventually yields a larger number of scales for a fixed value of  $n-m$ . Then, upon reconstructing the modified signal using Eq. (29), the artificially appended segment can be discarded. It is noted that for all practical cases the latter operation will have negligible impact on the response spectrum of the modified signal and thus on the matching with the design spectrum, since most of the signal energy would have been released at earlier times.

Fig. 7 provides a numerical example involving a single 40sec long artificial accelerogram belonging to the previously presented BWKT ensemble to further elucidate the above points. In particular, the quality of the matching between the response spectrum

of the seismic record  $D(T)$  and the target spectrum  $S_d(T)$  is gauged against the number of iterations performed in terms of the root-mean-squared error (RMS). That is, the

$$RMS\ error = \sqrt{\frac{1}{N_k} \sum_{j=1}^{N_k} \left( \frac{S_d(T_j) - D(T_j)}{S_d(T_j)} \right)^2} \quad (33)$$

is evaluated at  $N_k = 250$  equally spaced points on the interval  $[0.02, 5]$  of natural periods  $T$ . Note that evaluating the RMS error for  $T > 5$ sec does not serve the purpose of assessing the performance of the iterative matching procedure since at this range of periods the behavior of the response spectrum is primarily governed by the necessary baseline adjustments (see also Figs. 4-6). In Fig. 7a four harmonic wavelet bases of various scale widths ( $n-m$ ), constant at all frequencies are used for processing the same artificially augmented record by 10sec of total duration  $T_o = 50$ sec. In Fig. 7b, the difference  $n-m$  is fixed to 2, and the original signal with  $T_o = 40$ sec plus three other records zero-padded to various total durations are considered. As expected, use of smaller  $n-m$  values and/or larger signal durations  $T_o$  achieves better and faster convergence of the response spectrum to the target spectrum. This, of course, comes at the expense of increased computational effort per iteration.

Figs. 8 and 9 provide snapshots of the improved matching achieved by means of the proposed harmonic wavelet-based iterative scheme in terms of the displacement and the pseudo-acceleration spectra respectively for  $n-m=2$  and  $T_o = 50$ sec. Furthermore, Fig. 10 includes the acceleration, velocity and displacement time histories of the uncorrected and the baseline corrected record considered in Figs. 8 and 9 after 7 iterations. The obvious low-frequency unnatural trend of the displacement trace of the uncorrected accelerogram necessitates the use of high-pass filtering of the corresponding acceleration

trace. As discussed in section 2.3, an appropriate number of zeros have been appended in the beginning and at the end of the signal prior to the baseline adjustment [21]. These padded segments are maintained throughout the integrations to derive a suite of compatible acceleration, velocity, and displacement traces [40]. As can be inferred by Fig. 10, this need is justified by the fact that both the velocity trace and to a greater extent the displacement trace of the corrected accelerogram attain significant non-zero values during these initial and final appended segments. These values are artifacts that represent the end effects induced by the application of anti-causal filtering. However, their relatively small intensity has minor contribution to the response spectral ordinates [39].

#### *4.4 Adjustment of the Harmonic Wavelet basis to meet the EC8 compatibility criteria*

Noticeably, most of the contemporary regulations adopt compatibility criteria for artificial accelerograms to be used for the earthquake resistance design of structures significantly different from what Eq. (33) suggests. For a structure of fundamental natural period  $T_1$ , the EC8 requires considering a collection of at least three accelerograms obeying the following two rules: (a) The average of the zero period spectral response acceleration values calculated from the individual time histories should be greater than the product  $\alpha_g S$  (see also the Appendix), and (b) In the range of periods  $[0.2T_1, 2T_1]$  no value of the average response spectrum for 5% damping, calculated from all time histories, should be less than 90% of the corresponding value of the 5% damping design spectrum [22]. These rules can be mathematically expressed by the equations:

$$\frac{1}{N_s} \sum_{j=1}^{N_s} PGA_j > \frac{a_g S}{a_g S}, \quad (34)$$

and

$$\min_T \left\{ \frac{\frac{1}{N_s} \sum_{j=1}^{N_s} D_j(T)}{S_d(T)} \right\} > 0.90, \quad 0.2T_1 \leq T \leq 2T_1, \quad (35)$$

where  $N_s \geq 3$  is the number of accelerograms considered while  $PGA_j$  and  $D_j(T)$  are the peak ground acceleration and the displacement response spectrum of the  $j$ -th accelerogram, respectively.

Taking advantage of the versatility of the generalized harmonic wavelets, already discussed to some detail in section 3.2, a case-dependent wavelet base featuring scales of non-uniform bandwidths  $(n-m)\Delta\omega$  across the frequency axis can readily be constructed. The objective is to have a more detailed discretization of the frequency domain in the range of frequencies corresponding to the interval  $[0.2T_1 \ 2T_1]$  and a sparser grid outside this range. In this fashion, more weight is assigned to obtaining enhanced agreement of the response spectral ordinates of the accelerograms with the target spectrum for the oscillators whose natural frequencies lie closer to the fundamental period  $T_1$  of interest. This renders the iterative matching procedure much more efficient and cheaper in computational cost.

For instance, suppose a structure of fundamental natural period  $T_f = 1.5$  sec is to be designed for  $PGA = 0.36g$  and soil conditions B. Three arbitrarily selected accelerograms out of the previously generated BWKT ensemble are processed using Eq. (31) by means of a generalized harmonic wavelet basis with  $n-m = 1$  in the range of frequencies  $[2.09, 20.93]$  (rad/sec). This band corresponds to the range  $[0.3, 3]$  (sec) of periods, and  $n-m = 16$  for the rest of the frequencies considered. Appropriate 10sec long

zero-padding at the end of the records has been considered prior to the modification of the signals so that their total duration equals 50sec. This additional segment is completely removed, as previously explained, after the required spectrum matching is achieved and before any high-pass filtering for the baseline adjustment is made. After only four iterations the compatibility criteria of EC8 are satisfied for the baseline corrected artificial seismic signals. Specifically, the ratios of Eqs. (34) and (35) are computed as 1.19 ( $>1$ ) and 0.92 ( $>0.90$ ), respectively. The individual and the average displacement and pseudo-acceleration response spectra of the three thus obtained signals are shown in Fig. 11; Fig. 12 includes the acceleration, velocity and displacement traces these signals in the time domain.

## 5. Concluding remarks

A stochastic approach for simulating non-stationary strong ground motion records compatible with a given design displacement (target) spectrum in combination with a harmonic wavelet-based iterative procedure have been presented. Without loss of generality, the design spectrum prescribed by the European aseismic code provisions (EC8) has been exclusively considered in all numerical examples provided.

At first, a previously established in the literature stochastic method has been extended to relate in an approximate manner the target spectrum with a modulated evolutionary power spectrum (EPS), which is parametrically expressed by an analytical formula. This is accomplished by the use of a constant peak factor whose value has been calibrated via Monte Carlo simulations pertaining to the EC8 design spectrum. Upon determining the EPS, non-stationary artificial accelerograms compatible with the latter



spectrum have been synthesized using an appropriate auto-regressive-moving-average filter driven by white noise. It has been shown numerically that a reasonable agreement of the average response spectra of these accelerograms with the EC8 design spectrum can be achieved if the assumed spectral form of the EPS can effectively suppress the spurious low-frequency components of the underlying non-stationary process. In this respect, the Kanai-Tajimi power spectrum has been found rather inappropriate for the purpose, while the Clough-Penzien spectrum and a newly proposed Butterworth-filtered-Kanai-Tajimi spectrum constitute viable choices for defining the requisite EPS.

It is acknowledged that the initially determined stochastic model yields accelerograms whose frequency composition does not evolve with time, as is the case for usual recorded seismic signals. Nevertheless, it does possess a significant practical merit since it can yield any required number of design spectrum compatible artificial seismic accelerograms, “from scratch”, without the need of having access to any real records. Furthermore, it has been verified by numerically obtained EPSs associated with various levels of seismic intensity and for all soil types prescribed by the EC8 that the proposed approach captures reliably the site-specific soil conditions, as they are reflected in the EC8 design spectrum. Clearly these results, given in a tabular form, can facilitate the application of stochastic dynamics-based seismic risk assessment of contemporary constructed facilities.

Subsequently, the wavelet transform has been employed to decompose the simulated signals in a generalized harmonic wavelet basis of functions. In this regard, an iterative scheme has been used to process individually each of the decomposed signals to enhancing the agreement of its response spectrum with the target one. Further, it has been

shown how to take advantage of the unique attributes of harmonic wavelets to construct appropriately customized basis to efficiently treat small suites of simulated accelerograms for satisfying compatibility criteria for artificial accelerograms posed by the EC8.

Special attention has also been given in obtaining records possessing realistic velocity and displacement traces. In this respect, a state-of-the-art baseline correction technique, used in the processing of recorded accelerograms pertaining to actual seismic events, has been adopted. This step is critical for the design of extremely flexible structures or of structures expected to exhibit severe inelastic behavior. In fact, the attained values of the displacement spectral ordinates of the simulated records and thus their closeness to the corresponding target spectrum in the region of long periods is exclusively governed by the baseline adjustment considerations.

Obviously, the two distinct techniques presented in this study, namely the evolutionary power spectrum-based representation of the seismic severity and the subsequent wavelet-based iterative modification procedure of individual accelerograms can be used independently to address, as well, certain needs arising in the practice of aseismic design of structures. Specifically, the former may be used in conjunction with any appropriate stochastic dynamics technique (e.g. Monte Carlo-based [18] or statistical linearization-based [42]), for design scenarios necessitating the incorporation of the uncertainty attributes of the seismic hazard, explicitly. Further, the latter can be readily utilized to modify real recorded accelerograms in cases where accounting for the temporal evolution of the frequency content of strong ground motions is deemed essential. In both cases, the numerical results presented herein could be of particular merit for the aseismic design involving the EC8 regulations.

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## APPENDIX A

The elastic displacement response spectrum for oscillators with 5% ratio of critical damping and natural period  $T$ , is defined by the European aseismic code provisions (EC8) [22] by the expression

$$S_d(T) = \frac{1}{(2\pi)^2} \times \begin{cases} a_g S T^2 \left[ 1 + \frac{1.5T}{T_B} \right], & 0 \leq T \leq T_B \\ 2.5 a_g S T^2, & T_B \leq T \leq T_C \\ 2.5 a_g S T_C T, & T_C \leq T \leq T_D \\ 2.5 a_g S T_C T_D, & T_D \leq T \leq T_E \\ a_g S T_C T_D \left[ 2.5 - 1.5 \frac{T - T_E}{T_F - T_E} \right], & T_E \leq T \leq T_F \\ a_g S T_C T_D, & T \geq T_F \end{cases} \quad (A1)$$

In this equation,  $a_g$  is the peak ground acceleration (PGA),  $S$  is a soil-dependent amplification factor, and  $T_B$ ,  $T_C$ ,  $T_D$ ,  $T_E$ , and  $T_F$  are soil-dependent corner periods which define the various branches of the design spectrum, as shown in Figure A1. The values of these quantities for the five different types of soil considered in EC8 are included in Table A1.

Table 1. Parameters for the definition of various evolutionary power spectral forms compatible with the EC8 design spectrum for soil type B and peak ground acceleration  $a_g = 0.36g$  ( $g = 981 \text{ cm/sec}^2$ ).

KT spectrum [ $T_{min} = 0.02, T_{max} = 2$ ] (sec)	KT spectrum [ $T_{min} = 0.02, T_{max} = 4$ ] (sec)	BWKT spectrum [ $T_{min} = 0.02, T_{max} = 10$ ] (sec)	CP spectrum [ $T_{min} = 0.02, T_{max} = 10$ ] (sec)
$C = 19.05 \text{ cm/sec}^{2.5}$ $b = 0.51 \text{ sec}^{-1}$ $\zeta_g = 0.71$ $\omega_g = 14.27 \text{ rad/sec}$	$C = 7.66 \text{ cm/sec}^{2.5}$ $b = 0.25 \text{ sec}^{-1}$ $\zeta_g = 0.47$ $\omega_g = 15.34 \text{ rad/sec}$	$C = 17.20 \text{ cm/sec}^{2.5}$ $b = 0.45 \text{ sec}^{-1}$ $\zeta_g = 0.74$ $\omega_g = 14.03 \text{ rad/sec}$ $N = 2$ $\omega_o = 3.14 \text{ rad/sec}$	$C = 18.29 \text{ cm/sec}^{2.5}$ $b = 0.46 \text{ sec}^{-1}$ $\zeta_g = 0.78$ $\omega_g = 13.18 \text{ rad/sec}$ $\zeta_f = 0.88$ $\omega_f = 3.13 \text{ rad/sec}$

Table 2. Parameters for the definition of CP evolutionary power spectra compatible with various EC8 design spectra.

Peak ground acceleration	Soil type	CP power spectrum parameters [ $T_{min} = 0.02, T_{max} = 10$ ] (sec)					
		$C$ ( $\text{cm/sec}^{2.5}$ )	$b$ ( $1/\text{sec}$ )	$\zeta_g$	$\omega_g$ ( $\text{rad/sec}$ )	$\zeta_f$	$\omega_f$ ( $\text{rad/sec}$ )
$a_g = 0.24g$ ( $g = 981$ $\text{cm/sec}^2$ )	A	9.56	0.58	0.52	18.94	0.94	2.37
	B	13.99	0.54	0.71	13.84	0.96	2.43
	C	14.48	0.48	0.79	10.23	1.25	2.13
	D	22.84	0.50	0.89	7.16	1.17	2.12
	E	17.71	0.54	0.77	12.64	1.29	2.11
$a_g = 0.36g$ ( $g = 981$ $\text{cm/sec}^2$ )	A	15.16	0.60	0.56	18.80	0.93	2.43
	B	18.29	0.46	0.78	13.18	0.88	3.13
	C	21.05	0.48	0.80	10.95	0.92	2.47
	D	28.70	0.46	0.85	8.44	1.11	2.08
	E	24.04	0.50	0.75	13.11	1.21	2.19

Table A1. Soil-dependent parameters for the definition of the EC8 design spectrum [22].

Soil type	S	$T_B$ (sec)	$T_C$ (sec)	$T_D$ (sec)	$T_E$ (sec)	$T_F$ (sec)
A	1.00	0.15	0.40	2.00	4.50	10.00
B	1.20	0.15	0.50	2.00	5.00	10.00
C	1.15	0.20	0.60	2.00	6.00	10.00
D	1.35	0.20	0.80	2.00	6.00	10.00
E	1.40	0.15	0.50	2.00	6.00	10.00

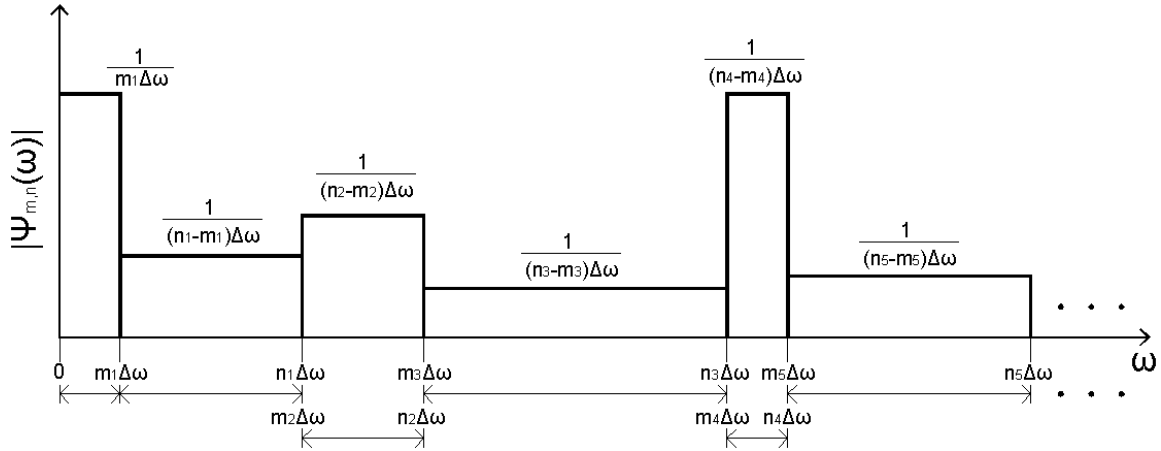


Fig. 1. An example of a generalized harmonic wavelets basis spanning non-overlapping intervals of arbitrary bandwidths in the frequency domain.

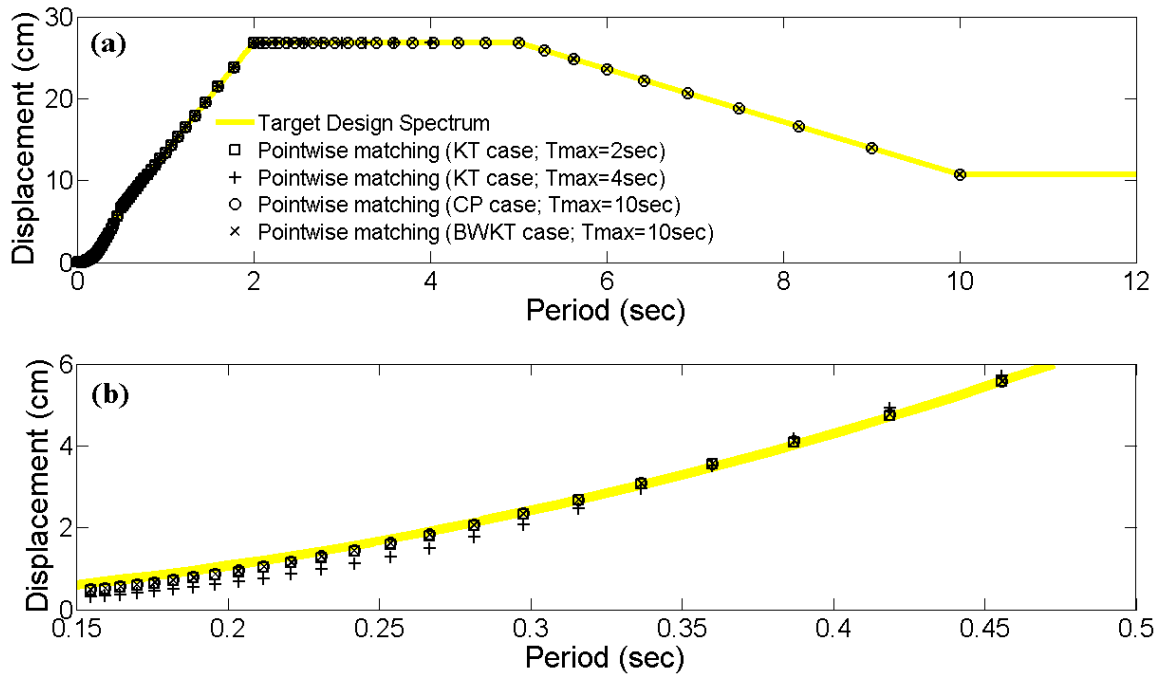


Fig. 2. Point-wise least square matching for the spectral forms considered in Table 1. Plot (b) zooms in plot (a) at the period interval  $[0.15, 0.45]$  (sec).



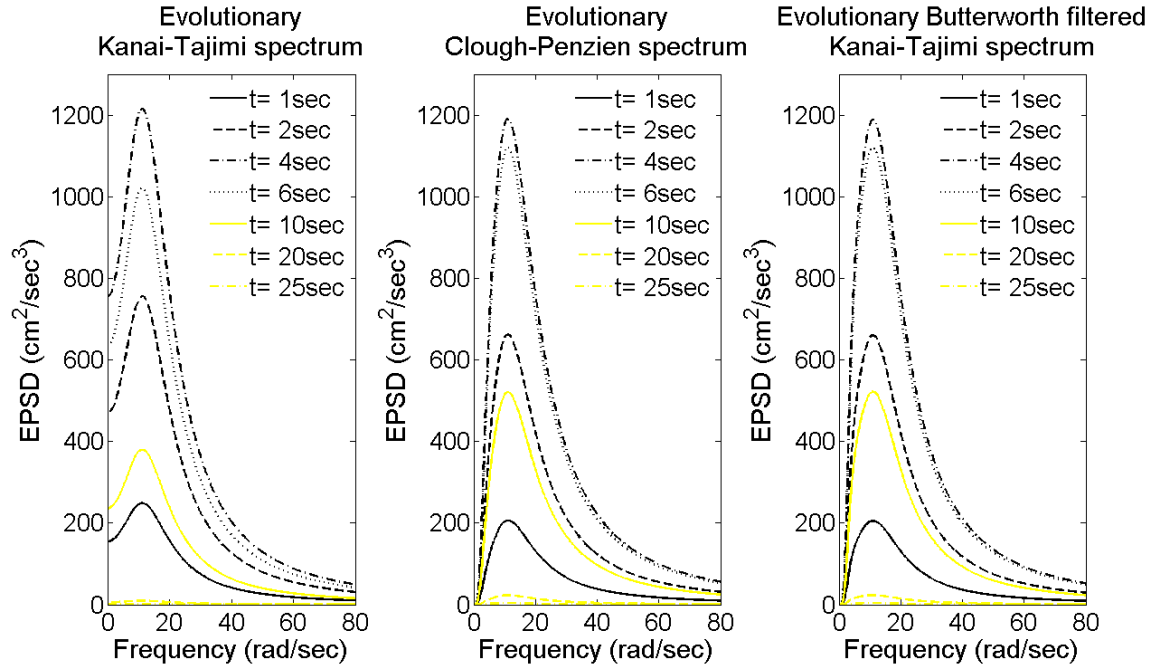


Fig. 3. Evolutionary power spectral forms given in Table 1. The plotted KT corresponds to the case of  $T_{max}=2\text{sec}$ .

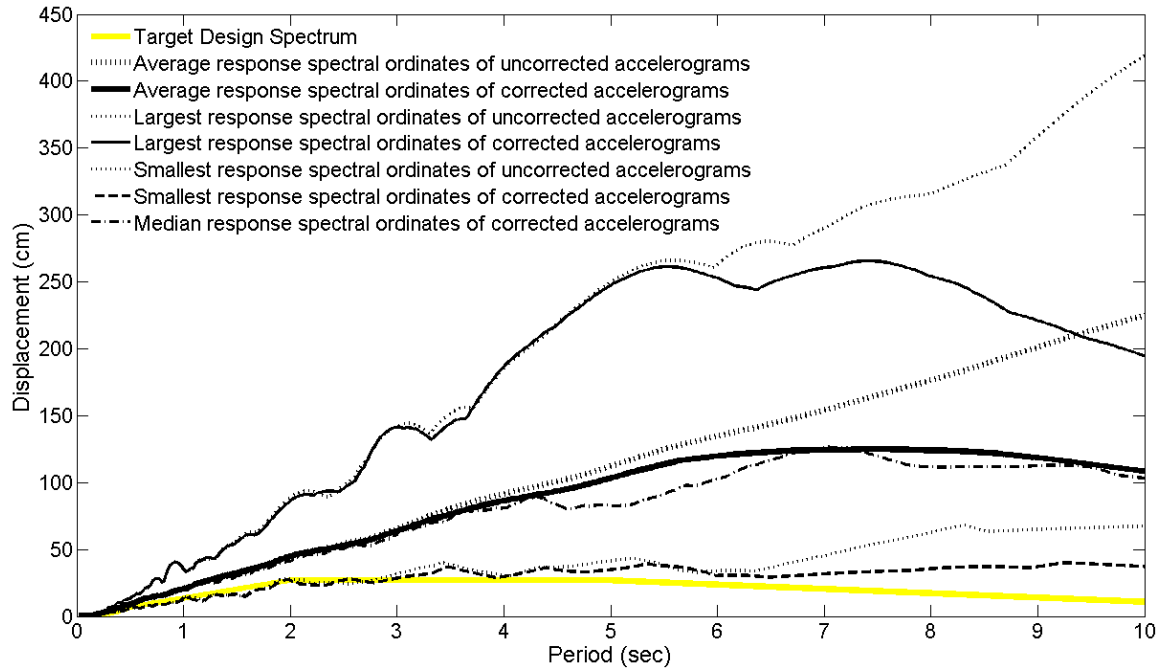


Fig. 4. Displacement response spectra of an ensemble of 40 simulated accelerograms compatible with the KT evolutionary power spectrum given in Table 1 for  $T_{max}=2\text{sec}$ .

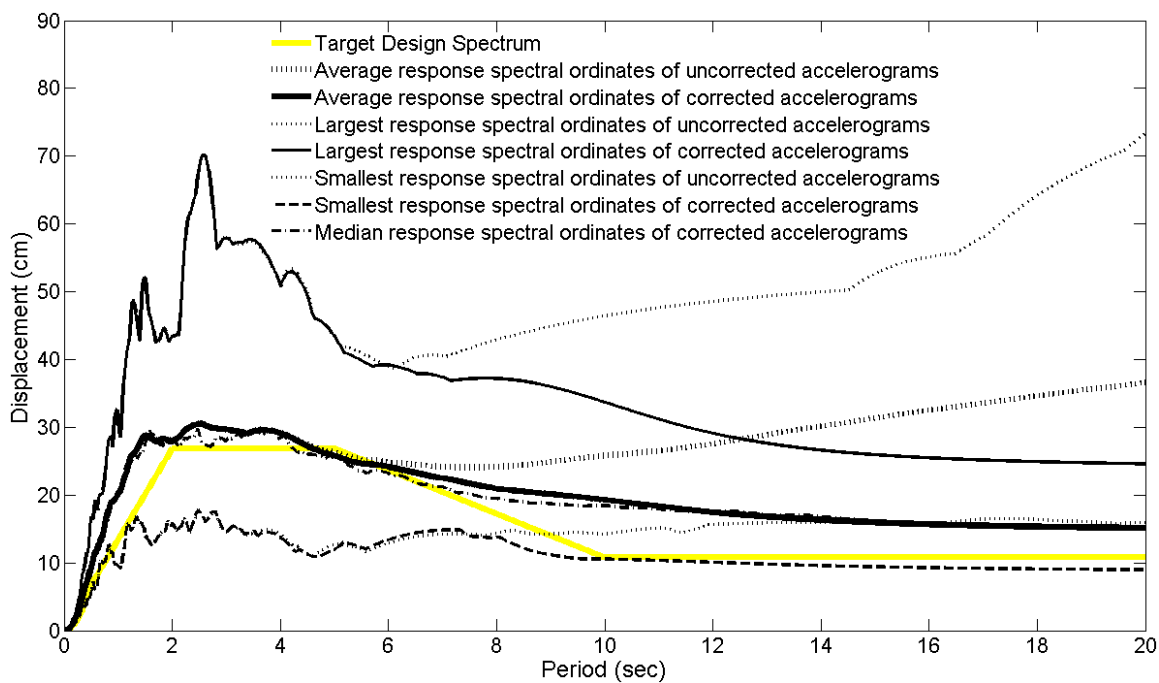


Fig. 5. Displacement response spectra of an ensemble of 40 simulated accelerograms compatible with the BWKT evolutionary power spectrum given in Table 1.

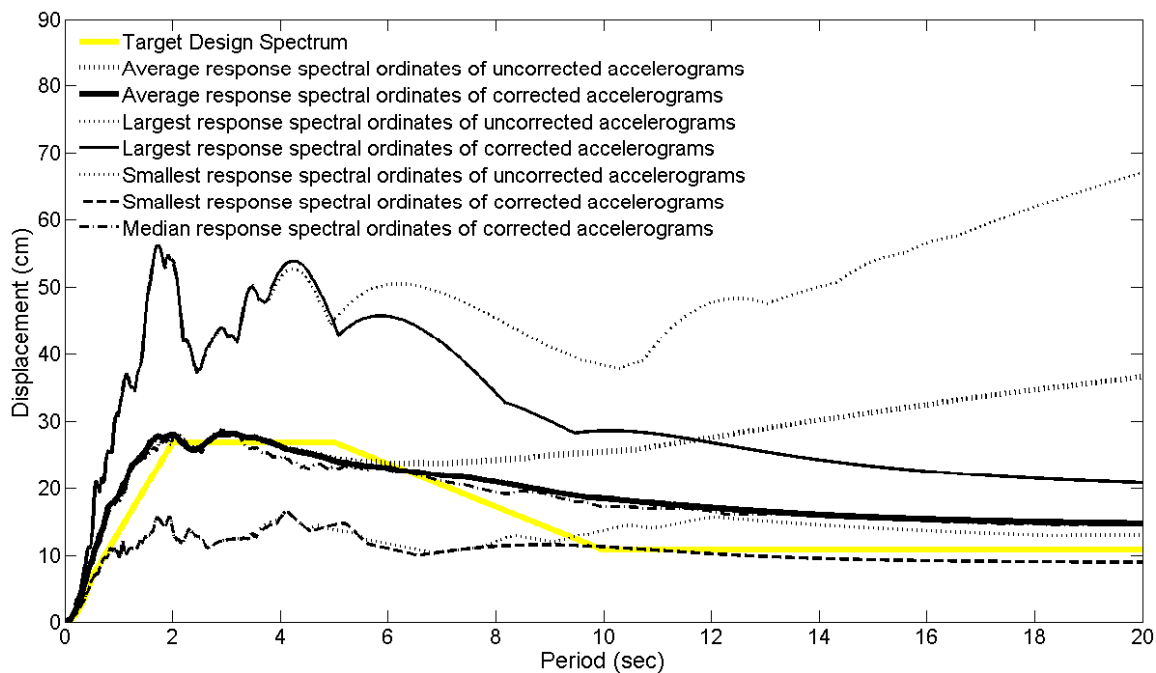


Fig. 6. Displacement response spectra of an ensemble of 40 simulated accelerograms compatible with the CP evolutionary power spectrum given in Table 1.

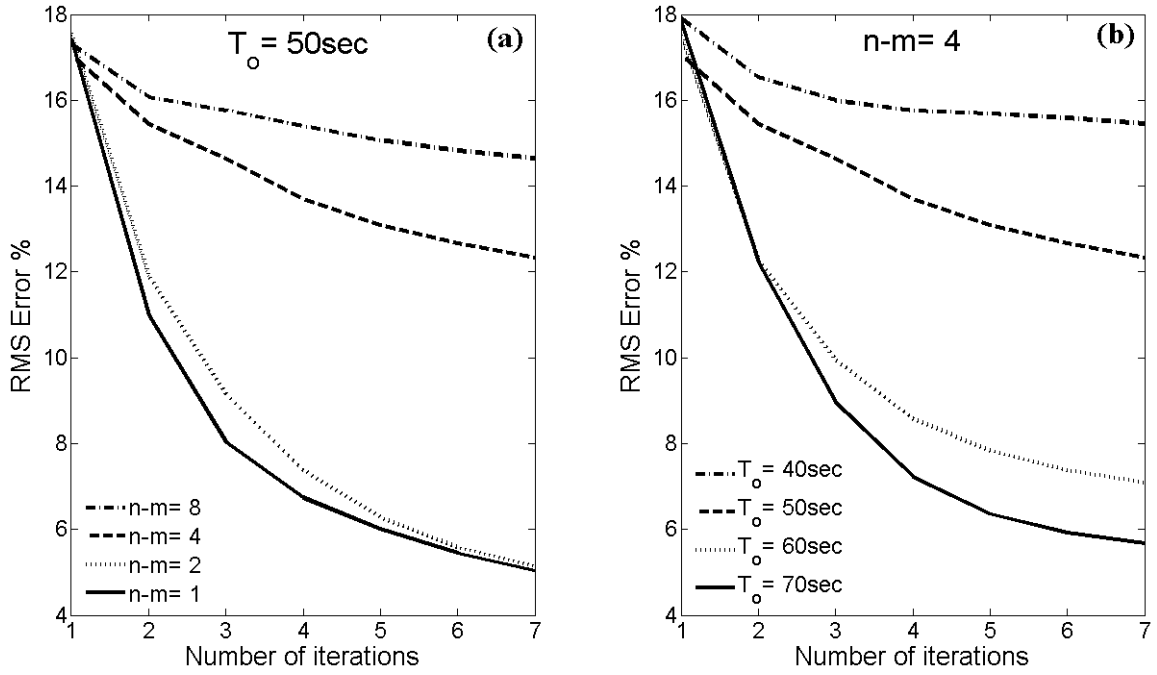


Fig. 7. Quality of matching of the response spectrum of an individual accelerogram with the target spectrum in terms of the RMS error (Eq. (33)) as a function of the number of iterations performed, the signal duration and the difference  $n-m$  in the construction of the harmonic wavelet base.

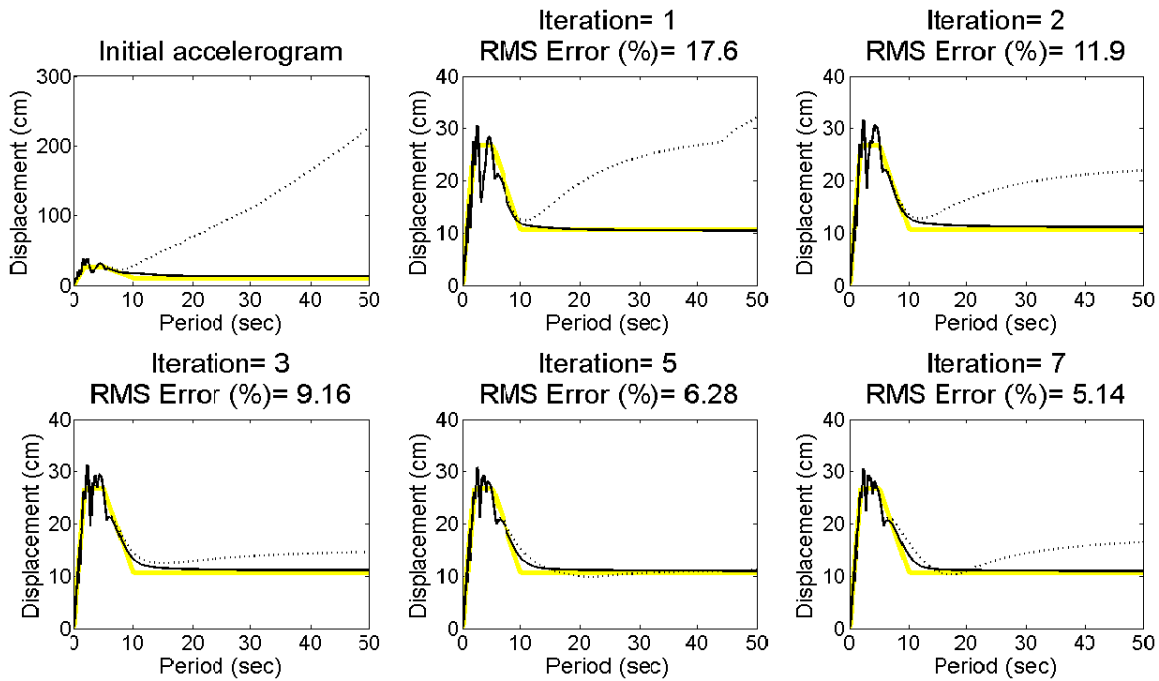


Fig. 8. Performance of the iterative matching procedure in terms of the displacement response spectrum of a single 50sec long accelerogram for uniform width of the harmonic wavelet basis  $n-m=2$ . Grey line: target spectrum; solid black line: response spectrum of the baseline corrected modified accelerogram; dotted black line: response spectrum of the uncorrected modified accelerogram.

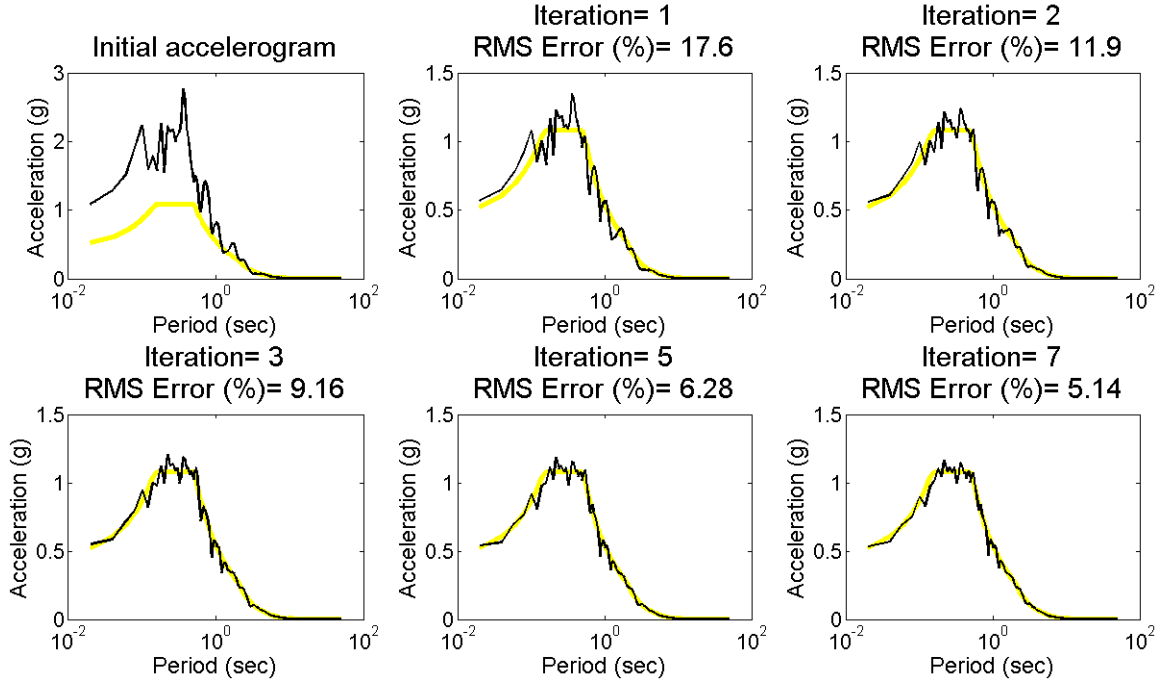


Fig. 9. Performance of the iterative matching procedure in terms of the pseudo-acceleration response spectrum of a single 50sec long accelerogram for uniform width of the harmonic wavelet basis  $n-m=2$ . Grey line: target spectrum; solid black line: response spectrum of the baseline corrected modified accelerogram; dotted black line: response spectrum of the uncorrected modified accelerogram.

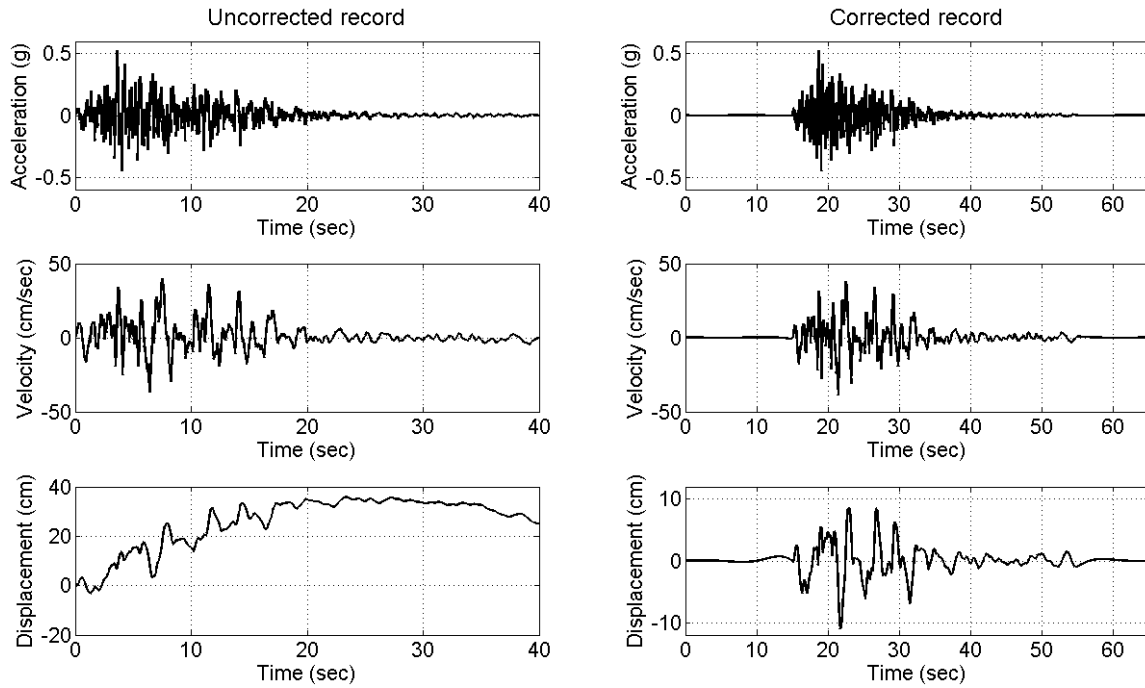


Fig. 10. Acceleration, velocity and displacement traces of the uncorrected and the baseline corrected record considered in Figs. 8 and 9 after 7 iterations.

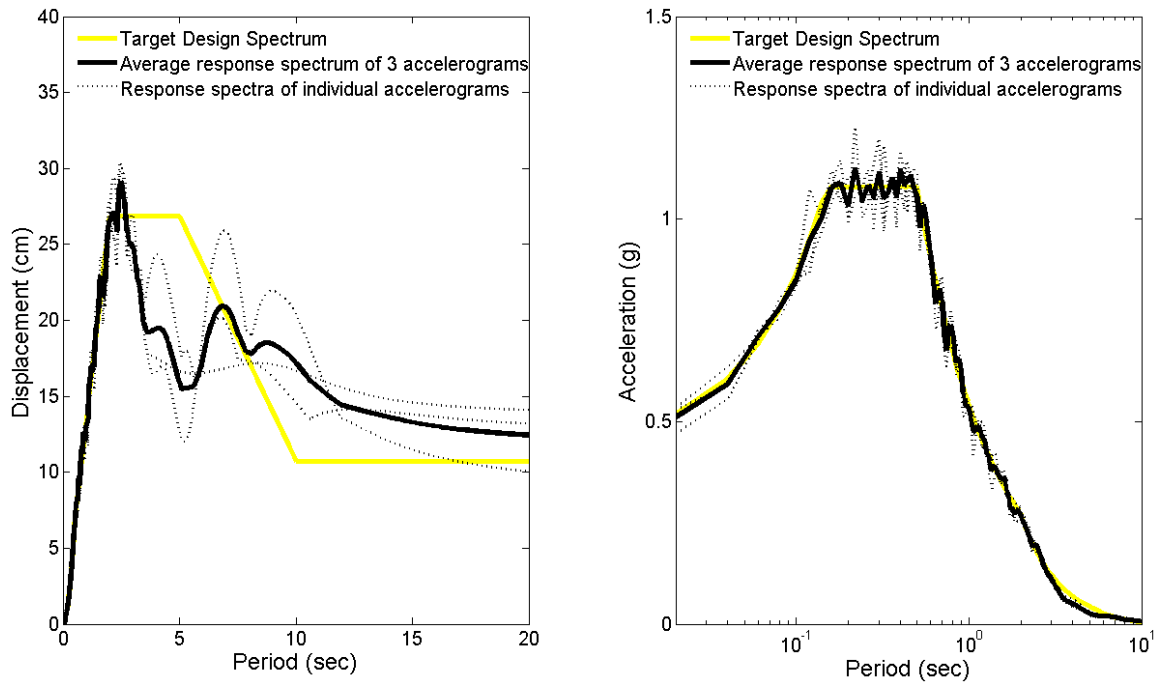


Fig. 11. Displacement and pseudo-acceleration response spectra of three base-line corrected accelerograms appropriately modified using a harmonic wavelet basis with non-uniform scale bandwidths ( $n-m$ ) to meet the compatibility criteria of EC8. Four iterations have been performed.

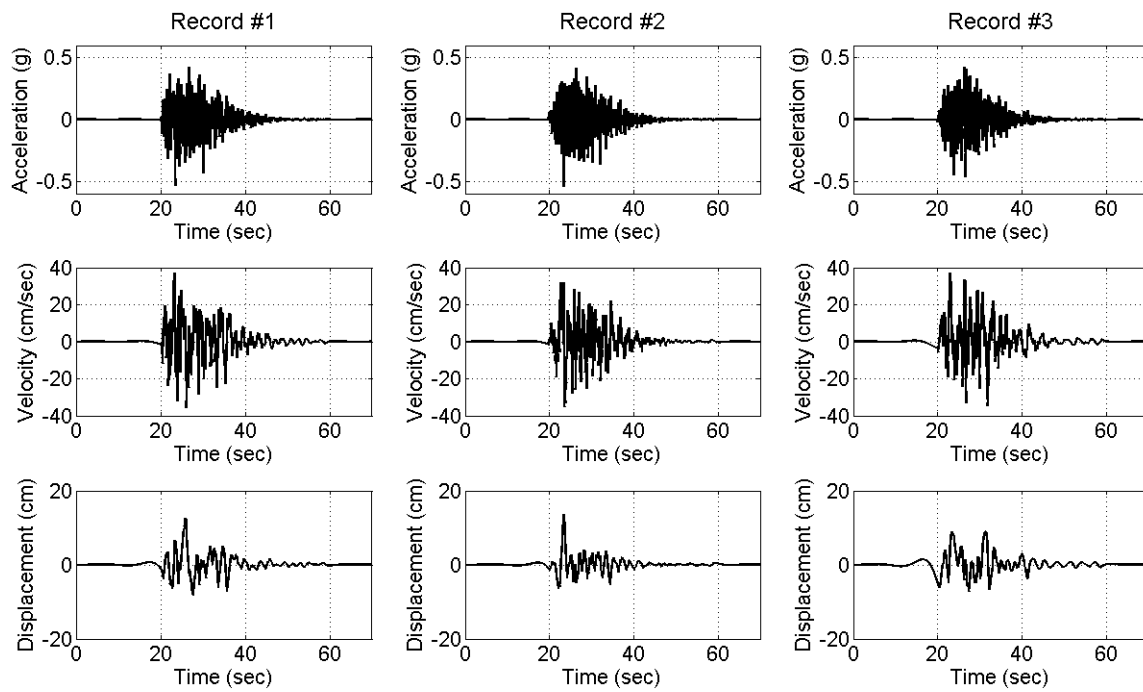


Fig. 12. Acceleration, velocity and displacement traces of three base-line corrected accelerograms appropriately modified using a harmonic wavelet basis with non-uniform scale bandwidths ( $n-m$ ) to meet the compatibility criteria of EC8. Four iterations have been performed.



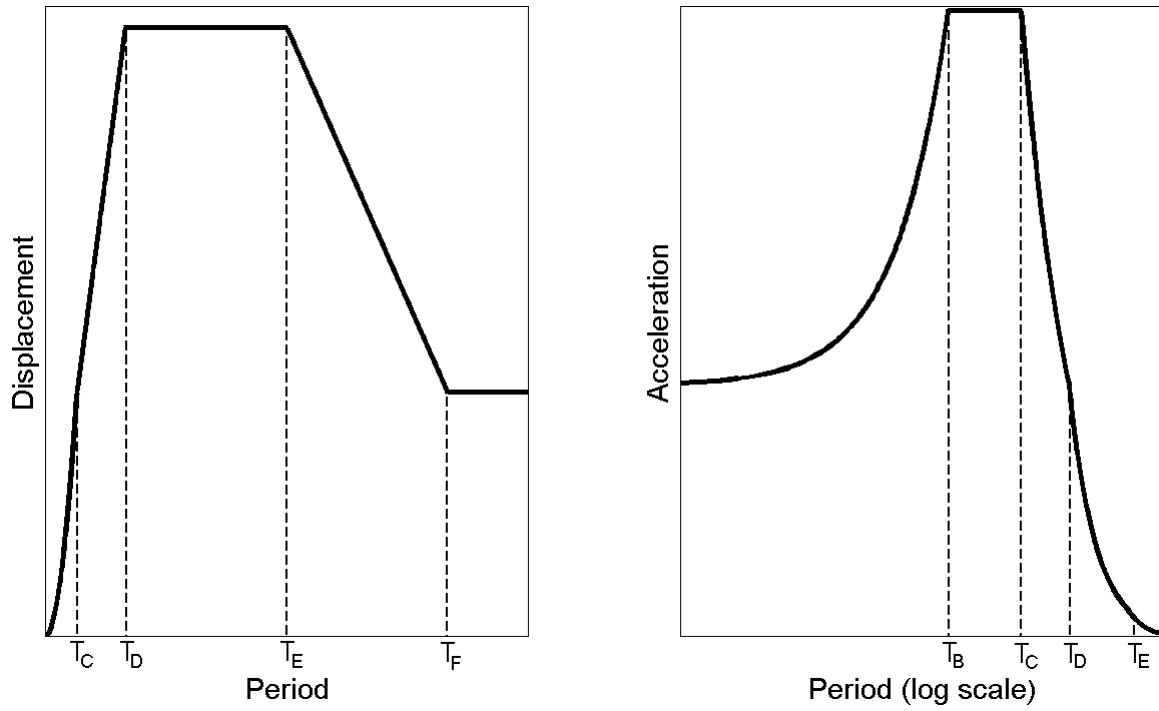


Fig. A1. Graphical representation of the elastic displacement and pseudo-acceleration design spectra of the EC8 [22].